## Revisions and Errata List <br> AISC Steel Design Guide 9, March 2015 Revision (Digital Edition) <br> February 16, 2023

The following list represents corrections to the digital edition, March 2015 revision, of AISC Design Guide 9, Torsional Analysis of Structural Steel Members.

## Page(s) Item

3

7

In the second column, the definition for $\theta^{\prime \prime}$, has a typographical error. It should be modified to read " $\theta$ '" $=$ third derivative of $\theta$ with respect to $z "$

In the last paragraph of Section 3.1, the first sentence has a typographical error. It should read, "In the above equations, $\theta^{\prime}, \theta^{\prime \prime}, \theta^{\prime \prime}$, and $\theta^{\prime \prime}$, , are the first, second, third, and fourth derivates of $\theta \ldots$ "

In the left column, beginning with the $5^{\text {th }}$ line from the bottom, replace the existing text as follows:

From Example 5.1,

$$
\begin{align*}
T_{u} & =\frac{-90 \mathrm{kip}-\mathrm{in} .}{2}=-45 \mathrm{kip}-\mathrm{in} . \\
\tau_{t} & =\frac{T_{u}}{2 t A_{o}}  \tag{4.4}\\
& =\frac{-45 \mathrm{kip}-\mathrm{in} .}{2(1 / 2 \mathrm{in} .)(9.5 \mathrm{in} . \times 5.5 \mathrm{in} .)} \\
& =-0.861 \mathrm{ksi}
\end{align*}
$$

In the right column, replace the first four lines with the following:

## Calculate Combined Stress

$$
\begin{align*}
f_{u v} & =\tau_{b}+\tau_{t}  \tag{4.10}\\
& = \pm 0.75 \mathrm{ksi}-0.861 \mathrm{ksi} \\
& =-1.61 \mathrm{ksi}
\end{align*}
$$

In the table at the top of the first column, the value of $f_{u v}$ for the TS10x $6 \times 1 / 2$ should be changed from 2.47 ksi to 1.61 ksi .

In Example 5.4 under the heading, Calculate Maximum Rotation, the calculations should be replaced with:

From Appendix B, Case 3 with $\alpha=0.3$, it is estimated that the maximum rotation will occur at 12.75 ft from the left end of the beam (Point A). At this location, $z / l=0.51$ for $T_{B}$ and $z / l=1-0.51=0.49$ for $T_{D}$. The service-load torques are:
$T_{B}=(210 \mathrm{kips})(3 \mathrm{in})=.630 \mathrm{kip}-\mathrm{in}$.
$T_{D}=(285 \mathrm{kips})(3 \mathrm{in})=.855 \mathrm{kip}-\mathrm{in}$.
The maximum rotation is

$$
\begin{aligned}
\theta & =0.064\left(\frac{T_{B} l}{G J}\right)+0.065\left(\frac{T_{D} l}{G J}\right) \\
& =0.064 \frac{(630 \mathrm{kip}-\mathrm{in} .)(300 \mathrm{in} .)}{(11,200 \mathrm{ksi})\left(107 \mathrm{in.} .^{4}\right)}+0.065 \frac{(855 \mathrm{kip}-\mathrm{in} .)(300 \mathrm{in.})}{(11,200 \mathrm{ksi})\left(107 \mathrm{in} .^{4}\right)} \\
& =0.024 \mathrm{rad}
\end{aligned}
$$

Replace the Case 2 graph with:



58-59 The torsional end restraints for the four Case $3 \alpha=0.1$ charts should be replaced with:

| Torsional End Restraints |  |
| :---: | :---: |
| Left End | Right End |
| Pinned $\theta=\theta^{\prime \prime}=0$ | Pinned $\theta=\theta^{\prime \prime}=0$ |

Replace the top graph for $\theta^{\prime \prime} \times\left(\frac{G J}{t}\right)$ with:


The variable description for the bottom graph should be revised to:

$$
\theta^{\prime \prime \prime} \times\left(\frac{G J}{t} \times \frac{10 a^{2}}{l}\right)
$$

Replace the top graph for $\theta \times\left(\frac{G J}{t} \times \frac{1}{a^{2}}\right)$ with:


Replace the bottom graph for $\theta^{\prime} \times\left(\frac{G J}{t} \times \frac{1}{a}\right)$ with:


Replace the top graph for $\theta^{\prime \prime} \times\left(\frac{G J}{t} \times 4\right)$ with:


Replace the bottom graph for $\theta^{\prime \prime \prime} \times\left(\frac{G J}{t} \times 2 a\right)$ with:


107 Equation C. 9 should be changed to:

$$
\theta=A+B z+C \cosh \frac{z}{a}+D \sinh \frac{z}{a}-\frac{t z^{3}}{6 G J}
$$

For Case 11, the equation for $\theta$ should be changed to:

$$
\theta=\frac{t a^{2}}{G J}\left\{1+\frac{l^{2}}{6 a^{2}}-\left(\frac{a}{l}+\frac{l}{2 a}\right) \tanh \frac{l}{a}-\frac{z}{l}+\left(\frac{a}{l}+\frac{l}{2 a}\right)\left(\frac{\sinh \frac{z}{a}}{\cosh \frac{l}{a}}\right)-\frac{z^{3}}{6 l a^{2}}\right\}
$$

