

AWS - AISC FILLET WELD STUDY

LONGITUDINAL AND TRANSVERSE
SHEAR TESTS

For

The American Institute of Steel Construction



Testing Engineers Incorporated

RR731

Materials Testing and Inspection

SANTA CLARA

OAKLAND

SAN DIEGO

Los Angeles

6851

LOS ANGELES



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May 31, 1968

AISC LIBRARY NEW YORK No. RR-731 Date 6/75

American Institute of Steel Construction 101 Park Avenue New York, New York 10017

Attention: Mr. T. R. Higgins

SUBJECT: AWS - AISC Fillet Weld Study

Gentlemen:

In accordance with your letter of authorization dated November 17, 1967, we have completed the fillet weld shear tests as outlined by the Joint AWS-AISC Advisory Task Group on Fillet Welds. Mr. Arsham Amarikian, Chairman.

These tests were conducted in our Oakland Laboratory under the direction of our Chief Metallurgist, Mr. Robert H. Kersten. Engineering supervision and report preparation was by the undersigned.

Also, in response to your verbal request, we have presented herein certain conclusions which in our opinion can be drawn from the results of this test program.

If you have any comments or questions on the conduct of the test or manner of reporting, please feel free to contact us.

Very truly yours,

TESTING ENGINEERS, INCORPORATED

Structural Engineer

FRP: csh

AWS - AISC FILLET WELD STUDY

LONGITUDINAL AND TRANSVERSE
SHEAR TESTS

REPORT OF TESTS

Ву

TESTING ENGINEERS, INCORPORATED

For

THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION

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AWS - AISC FILLET WELD STUDY

Longitudinal and Transverse Shear Tests

OBJECTIVE

To determine the ultimate strength of fillet welds subjected to longitudinal and transverse shear, the welds being manufactured under shop conditions by two fabricators, one eastern and one western, who were given instructions by the Joint AWS-AISC Task Group as to fabrication and identification of materials.

SCOPE

Longitudinal Shear Tests

Three test specimens each were tested in three sizes of fillet welds (1/4, 3/8, and 1/2 inch), four types of electrodes and three base materials from each of two fabricators requiring a total of 132 test specimens as shown in Table No. 1.

Transverse Shear Tests

Three 1/4-inch fillet weld test specimens each were tested using three types of electrodes and three basic materials from each of the two fabricators requiring a total of 36 test specimens as shown in Table No. 2.

TEST PROCEDURES

1. Identification

All specimens were shipped to our laboratory from the fabricators, prepared in accordance with Drawing D1 for longitudinal shear specimens and D4 for transverse shear specimens. Each specimen was steel-stamped by the fabricator at each end with the appropriate specimen number as shown in Table No. 1 and 2. Heat number of the base material was steel-stamped on the surface of each plate. These heat numbers and

TEST PROCEDURES (CONTINUED)

1. Identification (Continued)

corresponding specimen identification numbers were recorded by the inspection agency at the fabricators' shop on specimen data sheets, copies of which are retained in our files.

2. Machining

Upon receipt, sample identification marks were entered in data sheet form and samples were machined in our machine shop as shown on Drawing D2 for longitudinal fillet weld tests and D5 for transverse fillet weld tests. The gage length for each weld was measured and recorded to the closest hundredth of an inch prior to testing.

3. Testing

All weld specimens, longitudinal shear, transverse shear and base metal were tested in tension in accordance with A.S.T.M. A370 Mechanical Testing of Steel Products in our Baldwin 300,000 pound capacity Universal Testing Machine, calibrated in accordance with A.S.T.M. Designation E4-64.

4. Sectioning, Etching and Measuring

a. Longitudinal Fillet Welds

An additional transverse saw cut was made across the specimen, cutting all four welds in the remaining unstressed portion. This face was ground, polished and etched with a 20% solution of ammonium persulphate. After etching, the specimen was washed, dried and finally coated with clear plastic. After preparation, vertical and horizontal lines were scribed corresponding to the original plate surfaces as shown in Drawing D3.

Leg size "L_I" (horizontal) and "L_Z" (vertical) for all four etched fillet welds were measured and recorded. The actual throat dimension "T", defined as the shortest distance to the face of the weld from the intersection of the original plate surfaces was measured and recorded for all four welds as was the fracture width "W", which is defined as the average

4. Sectioning, Etching and Measuring (Continued)

a. Longitudinal Fillet Welds (Continued)

width of the fractured surface for the failed portion of the welds. See Drawing D-3. The distance edge to edge of the saw cuts for each weld was also measured and recorded as the gage length.

All measurements were taken with a machinist scale to the nearest hundredth of an inch. All measurements were later transcribed and included in this report under "Data Sheets - Longitudinal Fillet Welds".

b. Transverse Fillet Welds

The ends of each of eight unfailed fillet welds were acid etched as in 4a above. These welds were on the two outside edge pieces that remained after the three shear test specimens were cut from the large specimen plate shown in Drawing D4. All eight welds were measured and recorded to the nearest hundredth of an inch as required in Drawing D6. After fracture of the specimen, the measurements of the two fractured welds were transcribed and presented in this report under "Data Sheets - Transverse Fillet Welds".

5. Photography

Photomacrographs were taken to illustrate the following typical conditions:

Specimens "as-received" and after machining, manner of specimen identification, etched faces of machined sections showing scribed lines for measurement, and typical examples of failure showing weld distortion and failure surface.

RESULTS

- Measurements of weld dimensions in inches and failure loads in kips are recorded and reported on data sheets in the Appendix for longitudinal fillet welds, and separately for transverse fillet welds.
- Summary of calculated failure stresses based on three criteria are reported in Table No. 5 for longitudinal fillet welds and Table No. 6 for transverse fillet welds.

DISCUSSION OF RESULTS

Three general areas of interest in the results of these tests are developed: mode of failure, dimension of welds, including penetration, and strength of welds.

Modes of Failure

All specimens failed in the fillet welds.

The longitudinal fillet weld fracture surface typically originated at the roof and extended to the inclined surface of the weld at an angle less than 45° to the horizontal. Welds displayed high ductility in combined shear and torsional strains. The shearing distortion in some welds was approximately 10% of the length. The surface of failure appeared to be a short series of helical shaped tears. See photos no. 4 through 8 for typical failures. The specimens failed either at two welds on the same side of the splice or alternately in a lapped manner, see photos no. 4 and 5.

The transverse fillet weld fracture surface typically was at a flat angle from the horizontal and appeared to be a clean silky planar break, typically as shown in photo no. 13. Because of joint geometry, large shear distortions could not be measured, however, visual examination revealed a highly ductile failure surface. In practically all cases, the measured distance "W" of the fractured surface exceeded both the throat dimension "T" and the penetration distance "P". In many cases the fracture width "W" was as large as the leg dimension "L".

As an aid to understanding of the types of failure, Figure No. 1 has been included to show the two types of loading and a schematic representation of stresses. It should be noted that higher shear stresses are also present in the transverse fillet welds, and torsional bending stresses are also present in the longitudinal fillet welds.

Dimensions of Welds

The basic dimensions recorded are as shown in Drawing D3 and D6. The important dimensions for evaluation of fillet weld size however, are the leg dimensions " L_1 " and " L_2 ". It is noted in the instructions to the fabricator that the specimens were to be positioned for flat welding, in the hope that the leg dimensions " L_1 " and " L_2 " would be equal. There is some evidence collected to indicate that one shop for some sizes may not have

Dimension of Welds (Continued)

held strictly to this because the average of the horizontal legs was somewhat larger than the average of the vertical legs.

A statistical study was made of fillet weld leg dimension "L" and is presented herein in Figure No. 2. It is significant that the range for the 3/8" fillet welds considerably lapped over both ranges for the 1/4 inch and 1/2 inch fillets. More significant is that the range for the 1/2" fillet welds extended down to .35 inch and that there were more welds produced measuring 7/16" than either 3/8" or 1/2".

It is noteworthy that for the 1/4" fillet welds the average leg size was 20% over the specified; for 3/8" fillet welds the average leg size was 13% over that specified; and for 1/2" fillet welds the average leg size was only 5% over that specified.

It is also noted that only 15 out of 432 (3-1/2%) were less than the 1/4" specified; that 49 out of 336 (15%) were less than the 3/8" specified; and that 99 out of 288 (34%) were less than the 1/2" specified.

The coefficient of variation "V" and within test variation "V_t" appear to be reasonable for specimens prepared outside of laboratory control. We have insufficient information on quality evaluation of steel testing in general to rate these adequately.

A review of the data also substantiates previous accepted knowledge that, for these manually welded fillets, the penetration distance "P" seldom exceeds the measured throat "T". This is also shown in the typical photos no. 9 and 14.

Strength of Welds

The concept of strength for fillet welds differs considerably from groove welds which, because of geometry, are merely a continuation of the base metal. Joint configuration and direction of loads make fillet welds much more complicated in state of stress and deformation characteristics. This can be visualized readily by examination of Figure No. 1. The designer of fillet welded joints, however, normally need not concern himself with the state of stress, provided he can use a reasonable assumption as to what forces can be transferred safely from one plane to another. It is convenient to assume these forces are transferred in shear and to set a limit value which is called the

Strength of Welds (Continued)

allowable shear stress at the theoretical throat dimension of the nominal weld size. Using the allowable shear stress and multiplying it by the theoretical throat dimension, all allowable value can be determined for each size weld expressed in allowable force (kips) per lineal inch of weld.

The present AISC Code permits two values for allowable shear stresses in fillet welds. 13,600 psi is allowed for E60 manual electrodes on all steels or for E70 electrodes with A7 or A373 steels. 15,800 psi is allowed for E70 electrodes used on A36, A242 and A441 steels. The values in kips per lineal inch corresponding to these two criteria are plotted as dotted lines on the lower portion of Figure No. 3.

The average ultimate strength in longitudinal shear also expressed in kips per lineal inch is plotted in Figure No. 3 for the various combinations of electrodes, base material and weld size used in this test program. The values for transverse shear are plotted for the one size fillets tested (1/4"). Inspection of the "Tabulated Summary of Calculated Stresses" will reveal that transverse shear strengths for those combinations tested were from 40 to 70% more than corresponding values in longitudinal shear.

Failure stresses were calculated on the basis of three measured dimensions of the welds, namely the penetration distance "P", the throat dimension "T", and the fractured width "W". All of these calculated stresses are presented in the two sets of tables showing summary of calculated stresses. For comparison, the values for the eastern fabricated specimens are shown next to the values for the western specimens. By inspection, it was determined that the values calculated using fracture width "W" are consistently closer together (east and west) than are the values based on throat dimension or penetration dimension. Also, these are normally the least of the three values. Consequently, these values are plotted on Figure No. 4. The present Code allowable values are not plotted because of scale limitation.

Factors of Safety

Factors of safety were determined by dividing the ultimate shear strength (expressed in kips per lineal inch) by the existing allowable shear value (in kips per lineal inch). Two methods were used to calculate these factors. AWS-AISC Fillet Weld Study - Page 7

DISCUSSION OF RESULTS (CONTINUED)

Factors of Safety (Continued)

Method Λ was based on the average ultimate strength of six specimens.

Method B was based on the minimum individual strength of the six specimens.

Factors of safety for longitudinal fillet welds are presented in Table No. 3 and for transverse fillet welds in Table No. 4.

CONCLUSIONS

The following tentative conclusions can be reached as a result of this test program:

- Factors of safety for fillet welds appear to decrease with increasing weld size and do not increase in direct proportion to an increase in specified tensile strength of the materials used.
- Fillet weld size appears to be more closely related to the weld metal's ability to accommodate large shearing and bending strains rather than its being related to an arbitrary shear stress calculated on theoretical throat dimensions.
- The larger the size of manual fillet welds, the close the average measured size is to the specified size and the greater tendency there is for undersize welds.
- 4. Nevertheless, there appears to be ample room in the present factor of safety for a substantial increase in allowable stresses for fillet welds and to include the new high strength steels and electrodes now available, provided:
 - a. Adequate controls are exercised over dimension profile shape and other quality requirements.
 - Proper identification of base metals and electrodes is maintained during fabrication.

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CONCLUSIONS (CONTINUED)

5. It is apparent that if higher allowable stresses are permitted for fillet welds, smaller weld sizes would result, and size probably would be governed by the present requirements for minimum weld size as related to thickness of material used. Additional research is needed therefore, to establish a more rational basis for specifying this relationship. The need for such research, however, should not affect present deliberations on increasing allowable stresses.

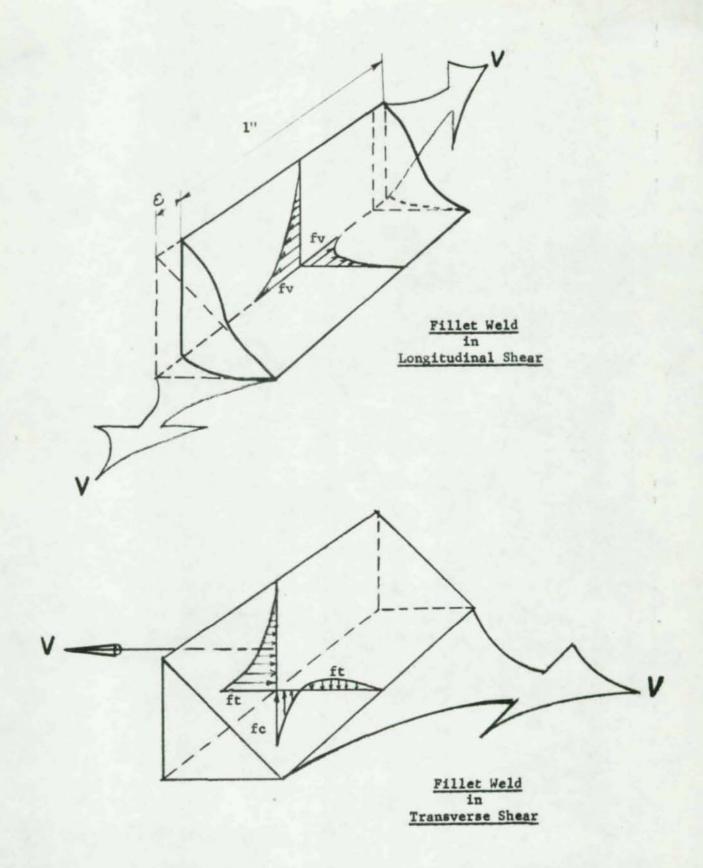
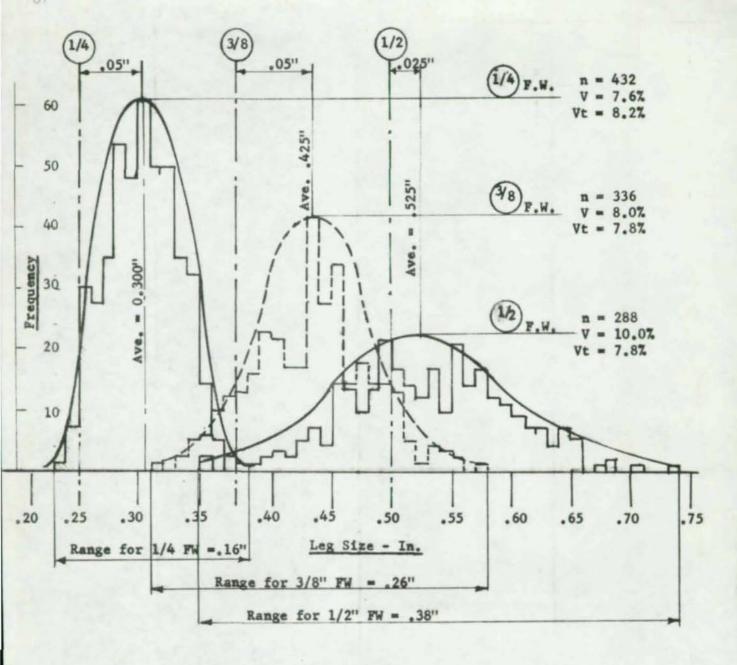


FIGURE NO. 1

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STATISTICAL VARIATION

IN

FILLET WELD LEG DIMENSION "L"

Representing a total of 132 samples with 4 measurements of horizontal legs and 4 measurements of vertical legs for each sample - 1056 measurements.

FIGURE NO. 2

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MECHANICAL TESTS

SPECIMEN

A.I.S.C. Fillet Weld Test Base metal used for specimens

A.S.T.M.	HEAT	SIZE AREA LOAD IN POUNDS	POUNDS	L85, PE	R SQ. IN.	ELONG	ATION	1000	NATURE OF	BEND TEST		
Desig.			SQ. IN.	POINT	MAXIMUM	POINT	TENSILE STRENGTH	2 IN IN.	PER CENT	IN/8 IN.	FRACTURE	0000
A-514	81P337	.780 × 1.544	1.204	131500	141250	109220	117320	.60	30.0	1.00	Silky	
A-514	73B665	.743 x 1.535	1.141	131000	141250	114810	123790	.64	32.0	1.01	Silky	
A-514	60B044	1.019 x 1.435	1.462	157000	171000	107390	116960	.69	34.5	1.03	Silky	
A-514	99P795	1.263 x 1.493	1.886	233250	250000	123670	132560	.61	30.5	.96	Silky	
A-514	66C281	.518 × 1.513	.784	80200	86600	102300	110450*	* .65	32.5	1.15	Silky	
							19					
							- 11					
	1,62	5.75	1				135.6					

REMARKS: West

* Failure

REPORTED TO:

** Retest

BY R. H. Kersten



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OAKLAND SAN JOSE LOS ANGELES SAN DIEGO

May 31, 1968

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American Institute of Steel Construction 101 Park Avenue

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Attention: Mr. T. R. Higgins

SUBJECT: AWS - AISC Fillet Weld Study

Gentlemen:

In accordance with your letter of authorization dated November 17, 1967, we have completed the fillet weld shear tests as outlined by the Joint AWS-AISC Advisory Task Group on Fillet Welds, Mr. Arsham Amerikian, Chairman.

These tests were conducted in our Oakland Laboratory under the direction of our Chief Metallurgist, Mr. Robert H. Kersten. Engineering supervision and report preparation was by the undersigned.

Also, in response to your verbal request, we have presented herein certain conclusions which in our opinion can be drawn from the results of this test program.

If you have any comments or questions on the conduct of the test or manner of reporting, please feel free to contact us.

Very truly yours,

TESTING ENGINEERS, INCORPORATED

Structural Engineer

FRP: csh

AWS - AISC FILLET WELD STUDY

LONGITUDINAL AND TRANSVERSE SHEAR TESTS

REPORT OF TESTS

Ву

TESTING ENGINEERS, INCORPORATED

For

THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION

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AWS - AISC FILLET WELD STUDY

Longitudinal and Transverse Shear Tests

OBJECTIVE

To determine the ultimate strength of fillet welds subjected to longitudinal and transverse shear, the welds being manufactured under shop conditions by two fabricators, one eastern and one western, who were given instructions by the Joint AWS-AISC Task Group as to fabrication and identification of materials.

SCOPE

Longitudinal Shear Tests

Three test specimens each were tested in three sizes of fillet welds (1/4, 3/8, and 1/2 inch), four types of electrodes and three base materials from each of two fabricators requiring a total of 132 test specimens as shown in Table No. 1.

Transverse Shear Tests

Three 1/4-inch fillet weld test specimens each were tested using three types of electrodes and three basic materials from each of the two fabricators requiring a total of 36 test specimens as shown in Table No. 2.

TEST PROCEDURES

Identification

All specimens were shipped to our laboratory from the fabricators, prepared in accordance with Drawing Dl for longitudinal shear specimens and D4 for transverse shear specimens. Each specimen was steel-stamped by the fabricator at each end with the appropriate specimen number as shown in Table No. 1 and 2. Heat number of the base material was steel-stamped on the surface of each plate. These heat numbers and

TEST PROCEDURES (CONTINUED)

1. Identification (Continued)

corresponding specimen identification numbers were recorded by the inspection agency at the fabricators' shop on specimen data sheets, copies of which are retained in our files.

2. Machining

Upon receipt, sample identification marks were entered in data sheet form and samples were machined in our machine shop as shown on Drawing D2 for longitudinal fillet weld tests and D5 for transverse fillet weld tests. The gage length for each weld was measured and recorded to the closest hundredth of an inch prior to testing.

3. Testing

All weld specimens, longitudinal shear, transverse shear and base metal were tested in tension in accordance with A.S.T.M. A370 Mechanical Testing of Steel Products in our Baldwin 300,000 pound capacity Universal Testing Machine, calibrated in accordance with A.S.T.M. Designation E4-64.

4. Sectioning, Etching and Measuring

a. Longitudinal Fillet Welds

An additional transverse saw cut was made across the specimen, cutting all four welds in the remaining unstressed portion. This face was ground, polished and etched with a 20% solution of ammonium persulphate. After etching, the specimen was washed, dried and finally coated with clear plastic. After preparation, vertical and horizontal lines were scribed corresponding to the original plate surfaces as shown in Drawing D3.

Leg size "L1" (horizontal) and "L2" (vertical) for all four etched fillet welds were measured and recorded. The actual throat dimension "T", defined as the shortest distance to the face of the weld from the intersection of the original plate surfaces was measured and recorded for all four welds as was the fracture width "W", which is defined as the average

4. Sectioning, Etching and Measuring (Continued)

a. Longitudinal Fillet Welds (Continued)

width of the fractured surface for the failed portion of the welds. See Drawing D-3. The distance edge to edge of the saw cuts for each weld was also measured and recorded as the gage length.

All measurements were taken with a machinist scale to the nearest hundredth of an inch. All measurements were later transcribed and included in this report under "Data Sheets - Longitudinal Fillet Welds".

b. Transverse Fillet Welds

The ends of each of eight unfailed fillet welds were acid etched as in 4a above. These welds were on the two outside edge pieces that remained after the three shear test specimens were cut from the large specimen plate shown in Drawing D4. All eight welds were measured and recorded to the nearest hundredth of an inch as required in Drawing D6. After fracture of the specimen, the measurements of the two fractured welds were transcribed and presented in this report under "Data Sheets - Transverse Fillet Welds".

5. Photography

Photomacrographs were taken to illustrate the following typical conditions:

Specimens "as-received" and after machining, manner of specimen identification, etched faces of machined sections showing scribed lines for measurement, and typical examples of failure showing weld distortion and failure surface.

RESULTS

- Measurements of weld dimensions in inches and failure loads in kips are recorded and reported on data sheets in the Appendix for longitudinal fillet welds, and separately for transverse fillet welds.
- Summary of calculated failure stresses based on three criteria are reported in Table No. 5 for longitudinal fillet welds and Table No. 6 for transverse fillet welds.

DISCUSSION OF RESULTS

Three general areas of interest in the results of these tests are developed: mode of failure, dimension of welds, including penetration, and strength of welds.

Modes of Failure

All specimens failed in the fillet welds.

The longitudinal fillet weld fracture surface typically originated at the roof and extended to the inclined surface of the weld at an angle less than 45° to the horizontal. Welds displayed high ductility in combined shear and torsional strains. The shearing distortion in some welds was approximately 10% of the length. The surface of failure appeared to be a short series of helical shaped tears. See photos no. 4 through 8 for typical failures. The specimens failed either at two welds on the same side of the splice or alternately in a lapped manner, see photos no. 4 and 5.

The transverse fillet weld fracture surface typically was at a flat angle from the horizontal and appeared to be a clean silky planar break, typically as shown in photo no. 13. Because of joint geometry, large shear distortions could not be measured, however, visual examination revealed a highly ductile failure surface. In practically all cases, the measured distance "W" of the fractured surface exceeded both the throat dimension "T" and the penetration distance "P". In many cases the fracture width "W" was as large as the leg dimension "L".

As an aid to understanding of the types of failure, Figure No. 1 has been included to show the two types of loading and a schematic representation of stresses. It should be noted that higher shear stresses are also present in the transverse fillet welds, and torsional bending stresses are also present in the longitudinal fillet welds.

Dimensions of Welds

The basic dimensions recorded are as shown in Drawing D3 and D6. The important dimensions for evaluation of fillet weld size however, are the leg dimensions "L1" and "L2". It is noted in the instructions to the fabricator that the specimens were to be positioned for flat welding, in the hope that the leg dimensions "L1" and "L2" would be equal. There is some evidence collected to indicate that one shop for some sizes may not have

Dimension of Welds (Continued)

held strictly to this because the average of the horizontal legs was somewhat larger than the average of the vertical legs.

A statistical study was made of fillet weld leg dimension "L" and is presented herein in Figure No. 2. It is significant that the range for the 3/8" fillet welds considerably lapped over both ranges for the 1/4 inch and 1/2 inch fillets. More significant is that the range for the 1/2" fillet welds extended down to .35 inch and that there were more welds produced measuring 7/16" than either 3/8" or 1/2".

It is noteworthy that for the 1/4" fillet welds the average leg size was 20% over the specified; for 3/8" fillet welds the average leg size was 13% over that specified; and for 1/2" fillet welds the average leg size was only 5% over that specified.

It is also noted that only 15 out of 432 (3-1/2%) were less than the 1/4" specified; that 49 out of 336 (15%) were less than the 3/8" specified; and that 99 out of 288 (34%) were less than the 1/2" specified.

The coefficient of variation "V" and within test variation " V_t " appear to be reasonable for specimens prepared outside of laboratory control. We have insufficient information on quality evaluation of steel testing in general to rate these adequately.

A review of the data also substantiates previous accepted knowledge that, for these manually welded fillets, the penetration distance "P" seldom exceeds the measured throat "T". This is also shown in the typical photos no. 9 and 14.

Strength of Welds

The concept of strength for fillet welds differs considerably from groove welds which, because of geometry, are merely a continuation of the base metal. Joint configuration and direction of loads make fillet welds much more complicated in state of stress and deformation characteristics. This can be visualized readily by examination of Figure No. 1. The designer of fillet welded joints, however, normally need not concern himself with the state of stress, provided he can use a reasonable assumption as to what forces can be transferred safely from one plane to another. It is convenient to assume these forces are transferred in shear and to set a limit value which is called the

Strength of Welds (Continued)

allowable shear stress at the theoretical throat dimension of the nominal weld size. Using the allowable shear stress and multiplying it by the theoretical throat dimension, all allowable value can be determined for each size weld expressed in allowable force (kips) per lineal inch of weld.

The present AISC Code permits two values for allowable shear stresses in fillet welds. 13,600 psi is allowed for E60 manual electrodes on all steels or for E70 electrodes with A7 or A373 steels. 15,800 psi is allowed for E70 electrodes used on A36, A242 and A441 steels. The values in kips per lineal inch corresponding to these two criteria are plotted as dotted lines on the lower portion of Figure No. 3.

The average ultimate strength in longitudinal shear also expressed in kips per lineal inch is plotted in Figure No. 3 for the various combinations of electrodes, base material and weld size used in this test program. The values for transverse shear are plotted for the one size fillets tested (1/4"). Inspection of the "Tabulated Summary of Calculated Stresses" will reveal that transverse shear strengths for those combinations tested were from 40 to 70% more than corresponding values in longitudinal shear.

Failure stresses were calculated on the basis of three measured dimensions of the welds, namely the penetration distance "P", the throat dimension "T", and the fractured width "W". All of these calculated stresses are presented in the two sets of tables showing summary of calculated stresses. For comparison, the values for the eastern fabricated specimens are shown next to the values for the western specimens. By inspection, it was determined that the values calculated using fracture width "W" are consistently closer together (east and west) than are the values based on throat dimension or penetration dimension. Also, these are normally the least of the three values. Consequently, these values are plotted on Figure No. 4. The present Code allowable values are not plotted because of scale limitation.

Factors of Safety

Factors of safety were determined by dividing the ultimate shear strength (expressed in kips per lineal inch) by the existing allowable shear value (in kips per lineal inch). Two methods were used to calculate these factors.

Factors of Safety (Continued)

Method A was based on the average ultimate strength of six specimens.

Method B was based on the minimum individual strength of the six specimens.

Factors of safety for longitudinal fillet welds are presented in Table No. 3 and for transverse fillet welds in Table No. 4.

CONCLUS IONS

The following tentative conclusions can be reached as a result of this test program:

- Factors of safety for fillet welds appear to decrease with increasing weld size and do not increase in direct proportion to an increase in specified tensile strength of the materials used.
- Fillet weld size appears to be more closely related to the weld metal's ability to accommodate large shearing and bending strains rather than its being related to an arbitrary shear stress calculated on theoretical throat dimensions.
- The larger the size of manual fillet welds, the close the average measured size is to the specified size and the greater tendency there is for undersize welds.
- 4. Nevertheless, there appears to be ample room in the present factor of safety for a substantial increase in allowable stresses for fillet welds and to include the new high strength steels and electrodes now available, provided:
 - a. Adequate controls are exercised over dimension profile shape and other quality requirements.
 - Proper identification of base metals and electrodes is maintained during fabrication.

CONCLUSIONS (CONTINUED)

5. It is apparent that if higher allowable stresses are permitted for fillet welds, smaller weld sizes would result, and size probably would be governed by the present requirements for minimum weld size as related to thickness of material used. Additional research is needed therefore, to establish a more rational basis for specifying this relationship. The need for such research, however, should not affect present deliberations on increasing allowable stresses.

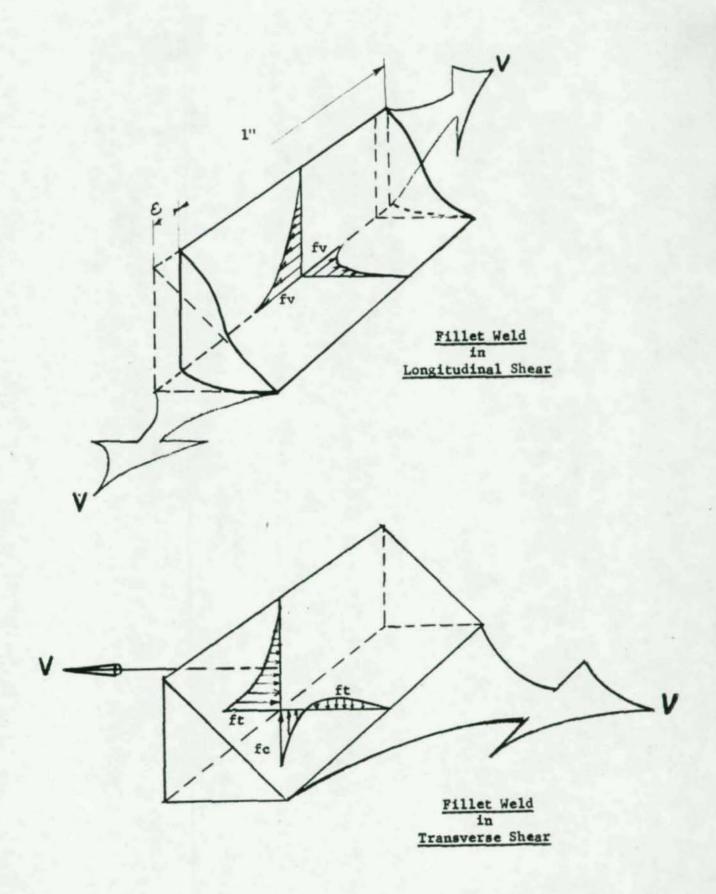
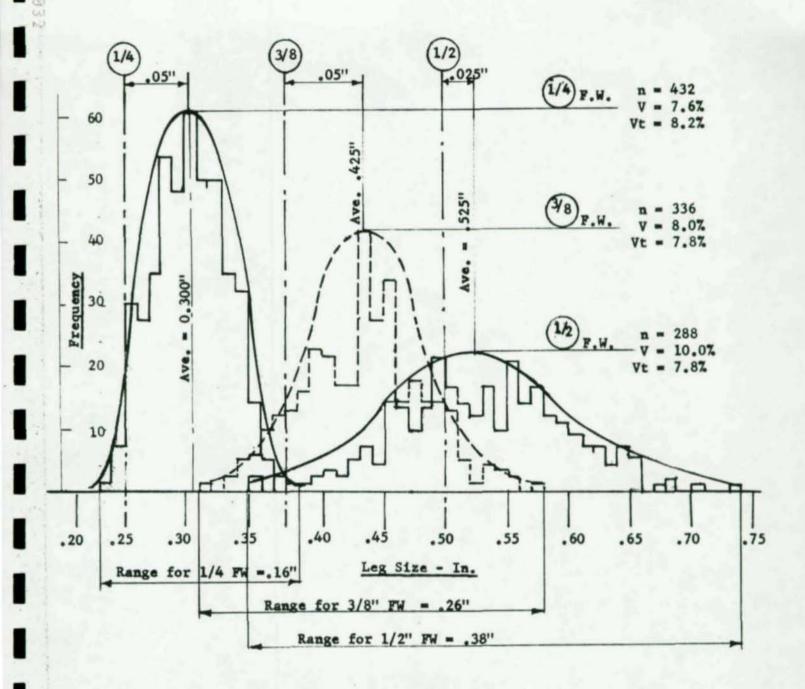


FIGURE NO. 1



STATISTICAL VARIATION

IN

FILLET WELD LEG DIMENSION "L"

Representing a total of 132 samples with 4 measurements of horizontal legs and 4 measurements of vertical legs for each sample - 1056 measurements.

FIGURE NO. 2

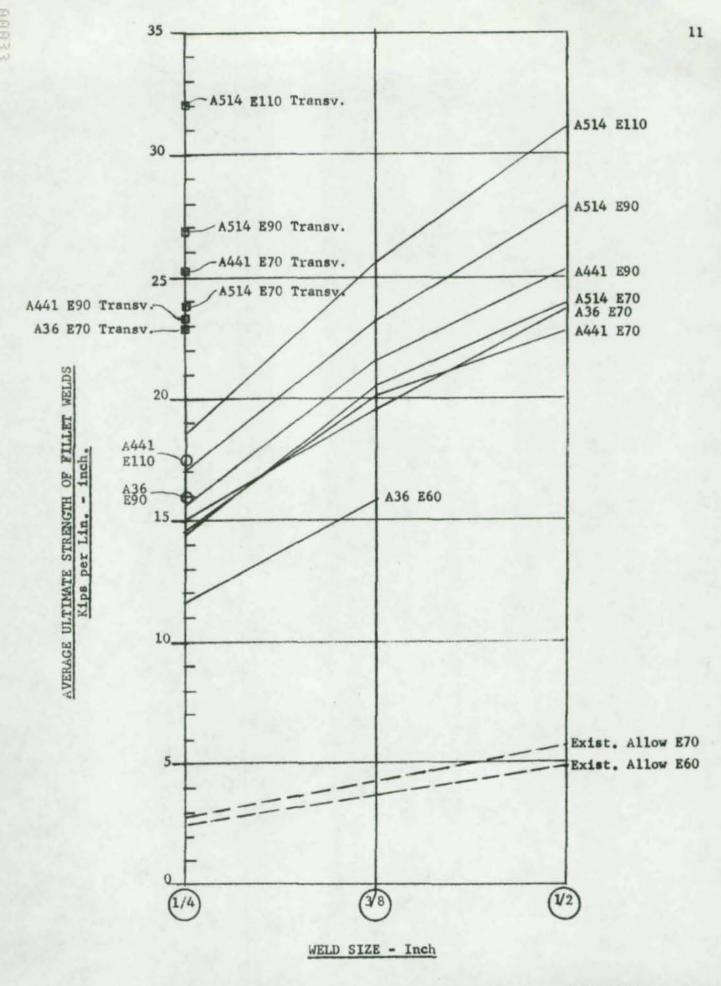
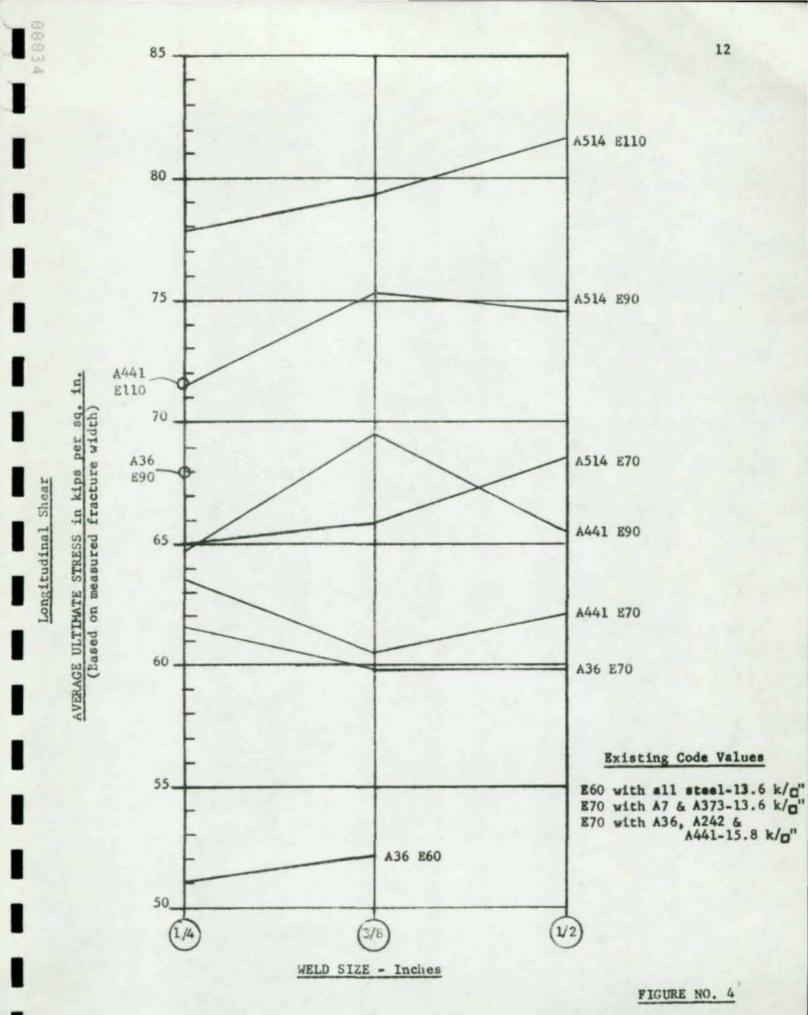


FIGURE NO. 3
TESTING ENGINEERS, INCORPORATED
Materials Testing and Inspection



TESTING ENGINEERS, INCORPORATED

Materials Testing and Inspection

TABLE I - SCHEDULE OF MATERIAL AND ELECTRODE COMBINATIONS AND IDENTIFICATION NUMBERS

	ELECTRODE	E-6	012		E-70 18		Section .	E-9018			E-110 18		
FABRICATOR	BASE SIZE	1/4"	3/8"	1/4"	3/8"	1/2"	1/4"	3/8"	1/2"	1/4"	3/8"	1/2"	
		W362A	W363A	W372A	W373A	W374A	W392A				and all Marie V		
	A-36	W362B	W363B	W372B	W373B	W374B	W392B		QUIRED				
		W362C	W363C	W372C	W373C	W374C	W392C						
WEST COAST				W472A	W473A	W474A	W492A	W493A	W494A	W412A			
(W)	A-441			W472B	W473B	W474B	W492B	W493B	W494B	W412B			
				W472C	W473C	W474C	W492C	W493C	W494C	W412C			
	A-514			W572A	W573A	W574A	W592A	W593A	W594A	W512A	W513A	W514A	
				W572B	W573B	W574B	W5928	W593B	W594B	W512B	W513B	W5148	
				W572C	W573C	W574C	W592C	W593C	W594C	W512C	W513C	W5140	
	A-36												
EAST COAST	A-441			L IDENTIFICATION NUMBERS ARE THE SAME AS ABOVE EXCEPT THE BRICATOR IDENTIFICATION, 'W' IS TO BE REPLACED BY 'E'					E				
	A-514												

NOTE - ONLY | SPECIMEN REQUIRED OF EACH IDENTIFICATION NUMBER

IDENTIFICATION NUMBER KEY

1ST DIGIT - FABRICATOR IDENTIFICATION -, "W" OR "E"

2ND DIGIT - BASE METAL IDENTIFICATION - 3 = A-36, 4 = A-441, 5 = A-514

3RD DIGIT - ELECTRODE TYPE - 7 = E70, 9 = E90, 1 = E110

4TH DIGIT - WELD SIZE - 2 = 1 4", 3 = 3/8", 4 = 1 2"

5TH DIGIT - SEQUENCE OF SAMPLE PREPARATION FOR EACH TYPE SPECIMEN - A B, & C

TABLE 2 - TRANSVERSE FILLET WELD TESTS

SCHEDULE OF MATERIAL - ELECTRODE COMBINATIONS AND IDENTIFICATION NUMBERS

ALL WELDS 1/4" FILLET WELDS

	BASE		ELECTRODE	
ABRICATOR	METAL	E70	E90	E110
		TW37A		
	A-36	TW37B		
		TW37C		No. of the last of
WEST		TW47A	TW49A	
COAST	A-441	TW47B	TW49B	
(W)		TW47C	TW49C	
		TW57A	TW59A	TW51A
	A-514	TW57B	TW59B	TW51B
		TW57C	TW59C	TW51C
		TE37A		
	A-36	TE37B		
EAST		TE37C		
		TE47A	TE49A	
COAST	A-441	TE47B	TE49B	7.00
(E)		TE47C	TE49C	
Links Links		TE57A	TE59A	TE51A
	A-514	TE57B	TE59B	TE51B
4 - 1 - 1 -		TE57C	TE59C	TE51C

IDENTIFICATION NUMBER KEY

1ST DIGIT = (T) MEANS TRANSVERSE WELD TEST

2ND DIGIT = FABRICATOR IDENTIFICATION, E OR W

3RD DIGIT = BASE METAL IDENTIFICATION 3 = A-36, 4 = A-441, 5 = A-514

4TH DIGIT - ELECTRODE IDENTIFICATION, 7 = E70, 9 = E90, 1 = E110

5TH DIGIT = SAMPLE NUMBER FOR EACH TYPE OF SPECIMEN

TABLE NO. 3

Factors of Safety Longitudinal Fillet Welds

Based on Existing Code Values 13.6 k/sq. in. for E60 15.8 k/sq. in. for all others

	Combination erial & Electrodes	1/4" F	illets	3/8" F	illets B	1/2" F	illets B
A36	E60	4.8	4.3	4.4	4.3		
	E70	5.3	5.1	4.6	4.4	4.2	4.2
A441	E70	5.3	5.0	4.8	4.4	4.1	3.8
	E90	5.5	4.7	5.2	5.0	4.5	4.3
A514	E70	5.2	4.6	4.9	4.5	4.2	3.8
	E90	6.1	5.3	5.5	5.1	5.0	4.4
	E110	6.6	5.6	6.1	5.3	5.7	5.1

Notes:

Column A is based on the Average ultimate strength (in kips per lin. inch) for 6 test specimens.

Column B is based on the Minimum ultimate strength (in kips per lin. inch) for 6 test specimens.

Factor of Safety is determined by dividing the ultimate shear strength (in kips/lin.) inch by the allowable shear value (in kips per lin. inch).

TABLE NO. 4

Factors of Safety Transverse Fillet Welds

Based on Existing Code Values - 15.8 k/sq. in.

		1/4" F	illets
Material Co Base Materi	mbination al & Electrode	Average	Minimum
A36	E70	8.2	7.6
A441	E70	9.0	8.5
A514	E70	8.5	7.2
A441	E90	8.4	6.8
A514	E90	9.6	8.6
A514	E110	11.5	9.7

SUMMARY OF CALCULATED STRESS LONGITUDINAL FILLET WELDS

SIZE	SPEC.	ST K	SQ. IN.*	Sp K/	SQ. IN.*	SW K/S	Q. IN.*	S K/L	.IN. IN.*
Base Metal Electrode	NO.	East	West	East	West	East	West	East	West
1.5	362A	68.2	48.1	57.3	49.8	48.5	49.8	13.5	10.6
1/4" A36	В	66.3	48.8	59.4	52.4	51.7	49.9	12.9	10.6
E60	С	65.6	47.4	56.3	50.2	55.8	52.1	13.9	10.4
Average		66.6	48.0	57.3	50.8	52.0	50.5	13.4	10.5
Av. E.W.		57	.3	54	.0	5	1.2	11	.5
3/8"	363A	55.4	47.9	55.8	48.2	48.2	54.1	15.9	15.6
A36 E60	В	55.6	48.2	53.3	48.2	50.1	54.1	16.4	15.7
200	С	59.0	50.9	56.8	53.9	54.8	53.0	15.8	16.0
Average		56.6	49.0	54.9	50.1	51.0	53.4	16.0	15.8
Av. E.W.		52	.8	52	.5	5:	2.2	15	.9
1/4"	372A	69.4	65.2	62.9	65.2	59.8	66.0	15.1	14.7
A36 E70	В	71.0	65.4	65.7	65.4	59.9	63.2	15.3	14.5
270	С	68.3	66.4	65.9	66.4	57.2	64.3	14.2	14.8
Average		69.5	65.6	64.8	65.6	58.9	64.4	14.8	15.3
Av. E.W.		67	.5	65	.2	6	1.6	15	.0
3/8"	373A	64.1	57.8	60.3	60.2	57.0	62.7	20.4	18.4
A36 E70	В	63.1	62.8	58.0	66.7	51.3	65.6	19.9	18.8
	С	63.8	61.5	60.5	61.5	56.4	66.9	20.6	18.9
Average		63.6	60.6	59.5	62.8	54.8	65.0	20.3	18.7
Av. E.W.		62	.1	61	.2	5	9.9	19	.5

*NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

Sw K/sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

LONGITUDINAL FILLET WELDS

SIZE	SPEC	ST K/	SQ. IN.*	Sp K/S	Q. IN.*	SW K/S	9. IN.*	S K/L	.IN. IN.*
Base Metal Electrode	NO.	East	West	East	West	East	West	East	West
1/2"	374A	64.4	60.8	55.9	60.8	59.1	60.8	23.5	23.4
A36 E70	В	65.4	60.8	57.1	61.2	58.5	62.4	23.7	23.4
	С	62.3	59.9	56.9	61.1	56.3	61.9	24.6	23.4
Average		64.0	60.5	56.6	61.0	57.9	61.7	23.9	23.4
Av. E.W		62	.3	59	.4	59	.8	23	.6
1/4"	392A	74.4	65.1	61.3	67.3	59.5	68.8	15.6	15.0
A36 E90	В	74.3	79.0	65.0	81.0	62.6	74.5	16.9	16.4
270	С	77.9	67.2	69.8	73.4	65.0	70.2	16.8	15.8
Average		75.7	70.4	65.4	73.9	62.4	71.2	16.4	15.8
Av. E.W		73	.0	69	.6	68	.0	16.	1
1/4"	472A	74.7	57.8	69.6	56.7	60.2	67.9	15.5	14.6
A441 E70	В	73.4	61.1	67.7	61.1	59.8	67.9	15.2	13.9
	c	68.8	63.4	64.6	62.7	61.4	63.4	15.6	14.4
Average		72.3	60.8	67.3	60.2	60.5	66.4	15.4	14.3
Av. E.W		66	.5	63	.8	63	.5	14.	.8
3/8"	473A	66.5	63.8	65.5	65.4	59.6	64.3	21.8	19.3
A441 E70	3	70.4	60.4	60.5	61.4	56.1	61.9	21.5	18.4
	c	68.2	57.0	60.3	59.8	59.9	61.7	22.2	18.7
Average		68.4	60.4	62.1	62,2	58.5	62.6	21.5	18.8
Av. E.W		64	.4	62	. 2	60	.5	20.2	

* NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

SW K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

LONGITUDINAL FILLET WELDS

SIZE	SPEC	ST K	'SQ. IN.*	Sp K/	SQ. IN.*	SW K/S	Q. IN.*	S K/I	.IN. IN.*
Base Meta Electrode		East	West	East	West	East	West	East	West
1/2"	474A	64.6	54.9	58.1	55.9	59.1	63.0	24.2	21.3
A441 B70	В	65.5	58.5	57.8	57.4	58.4	65.6	24.6	21.8
	С	62.1	58.5	59.0	60.1	59.4	64.2	23.9	21.3
Average		64,1	57.3	58.3	57.8	58.9	64.3	24.2	21.5
Av. E.W		60	.7	58	.0	62	.1	22.	8
1/4"	492A	79.0	63.7	68.2	65.3	62.7	67.0	17.6	13.1
A441 E90	В	76.5	69.4	65.4	68.6	63.5	74.7	16.8	14.6
	С	85.8	65.9	75.1	67.5	61.8	70.0	16.5	14.2
Average		80.4	66.3	69.6	67.1	62.7	70.6	16.9	14.0
Av. E.W		73	.3	68	.3	64.7 1: 67.6 72.6 22.0		15.	5
3/8"	493A	82.9	67.9	68.6	69.6	67.6	72.6	22.0	21.2
A441 E90	В	83.9	74.2	69.3	73.3	65.6	75.3	21.8	22.6
	С	73.0	71.5	66.3	71.5	65.8	71.5	21.5	20.8
Average		79.6	71.2	68.1	71.5	66.3	73,1	21.8	21.5
Av. E.W		75	.4	69	.6	69	.7	21.	7
1/2"	494A	81.5	66.9	70.9	67.8	61.2	70.7	25.9	25.1
A441 E90	В	79.9	67.4	65.2	67.4	60.2	71.3	25.6	24.8
	C	82.0	64.0	65.5	64.0	59.2	69.5	26.0	24.3
Average		81.1	66.1	67.2	66.4	60.2	70.5	25.8	24.7
Av. E.W		73	.6	66	.8	65	.4	25.	2

* NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

Sw K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

LONGITUDINAL FILLET WELDS

SIZE	SPEC.	ST K	SQ. IN.*	Sp K/	SQ. IN.*	SW K/S	Q. IN.*	S K/I	.IN. IN.*
Base Meta Electrode		East	West	East	West	East	West	East	West
1/4"	412A	83.4	63.7	76.7	65.4	70.9	64.5	19.0	12.4
A441 B110	В	88.4	69.2	85.4	77.4	72.9	70.9	18.8	14.7
	С	96.3	76.6	77.2	78.6	71.5	77.6	19.5	15.3
Average		89.4	69.8	79.8	73.8	71.8	71.0	19.1	14.1
Av. E.W.		79	.6	76	. 8	71	.4	16.	6
1/4"	572A	73.4	70.2	71.7	72.2	63.2	64.9	16.0	12.8
A514 E70	В	82.1	66.6	77.4	66.6	66.7	64.2	16.8	13.0
	С	75.2	70.0	73.4	75.1	64.4	66.3	15.8	12.8
Average		76.9	68.9	74.2	71.3	64.8	65.1	16.2	12.9
Av. E.W		72	.9	72	.8	65	.0	14.	.5
3/8"	573A	81.1	61.7	74.5	63.3	65.2	66.6	20.7	19.1
A514 E70	В	77.7	62.2	68.7	60.4	60.2	70.7	20.8	20.8
270	C	75.8	61.7	71.2	61.2	62.6	70.0	20.7	20.8
Average		78.2	61.9	71.5	61.6	62.7	69.1	20.7	20.2
Av. E.W		70	.0	66	.6	65.	.9	20.	4
1/2"	574A	70.6	63.5	69.2	64.0	69.6	71.7	25.9	22.2
A514 E70	В	74.6	64.7	68.4	63.2	71.1	68.8	26.5	21.7
	c	64.8	62.6	60.0	62.6	63.1	68.3	24.4	22.5
Average		70.0	63.6	65.9	63.2	67.9	69.6	25.6	22.1
Av. E.W		66	.8	64	.6	68.	.6	23.	.8

* NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

Sw K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

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TABLE 5 (CONT.) SUMMARY OF CALCULATED STRESS

LONGITUDINAL FILLET WELDS

SIZE	SPEC	ST K/	SQ. IN.*	Sp K/S	9. IN.*	SW K/S	Q. IN.*	S K/L	.IN. IN.*
ase Metal Electrode	NO.	East	West	East	West	East	West	East	West
1/4"	592A	88.6	79.6	82.0	79.6	68.8	73.7	19.3	14.9
A514 E90	В	89.8	75.6	82.7	73.8	66.3	78.5	18.4	15.1
	С	86.2	75.0	79.1	73.2	72.3	72.3	19.0	15.0
Average		88.2	76.7	81.3	75.5	69.1	73.8	18.9	15.0
Av. E.W		82	.5	78	.4	71	.5	17.	.0
3/8"	593A	82.6	69.6	74.2	69.1	74.8	78.0	23.7	22.6
A514 E90	В	85.1	71.7	76.8	75.4	71.0	75.4	23.6	22.4
	С	82.6	73.3	73.6	73.3	71.9	80.4	23.6	22.9
Average		83.4	71.5	74.9	72.6	72.6	77.9	23.6	22,6
Av. E.W		77	.5	73	.8	75	.2	23.	.1
1/2"	594A	81.9	72.6	74.9	72.1	73.1	76.5	30.7	24.9
A514 E90	В	83.2	72.4	77.8	73.5	70.2	77.4	30.4	25.4
	С	78.4	72.6	70.7	72.1	74.1	76.5	30.6	24.9
Average	, IB	81.2	72.5	74.5	72.6	72.5	76.8	30.6	25.1
Av. E.W		76.	9	73	.6	74	.6	27.	9
1/4"	512A	94.7	82.5	85.2	82.5	76.8	72.9	21.3	15.7
A514 E110	В	92.9	85.8	77.4	90.7	74.0	83.6	20.9	16.1
	Ç	99.4	80.1	92.7	79.2	79.5	81.1	20.9	16.2
Average		95.7	82.8	85.1	84.1	76.7	79.2	21.0	16.0
Av. E.W	1	89	.1	84	.8	77	.9	18.	.5

* NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. in. - ultimate stress based on measured penetration P

Sw K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

LONGITUDINAL FILLET WELDS

SIZE	SPEC.	ST K/	SQ. IN.*	Sp K/	SQ. IN.*	SW K/S	Q. IN.*	S K/1	.IN. IN.*
Base-Metal Electrode	NU.	East	West	East	West	East	West	East	West
3/8"	513A	100.8	74.1	91.6	77.3	76.9	73.5	27.5	22,4
A514 E110	В	100.3	81.2	86.2	79.9	77.2	82.5	27.6	25.0
	С	104.6	76.9	97.2	78.8	86.4	78.8	27.2	24.4
Average		101.9	77.4	91.6	78.7	80.2	78,3	27.4	23.9
Av. E.W.		89	.6	85	.2	79	.3	25	5.6
1/2"	514A	90.8	79.5	84.6	79.5	80.2	80.0	34.5	28.8
A514 E110	В	90.1	83.9	86.8	83.9	83.3	81.1	35.6	29.6
	С	90.0	84.5	87.2	86.3	80.1	84.5	34.4	30.0
Average		90.3	82.6	86.2	83.2	81.2	81.9	34.8	29.5
Av. E.W		86	.5	84	.7	81	.6	32	2.2
					3 3%				
Average				4-7	-64				
Av. E.W					844				
Average								1 3	
Av. E.W									

* NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

Sw K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

TABLE 6 SUMMARY OF CALCULATED STRESS

14" TRANSVERSE FILLET WELDS

SIZE		ST K/	SQ. IN.*	Sp K/S	Q. IN.*	SW K/SE	. IN.*	S K/1	.IN. IN.*
Base-Meta Electrode	4	East	West	East	West	East	West	East	West
	T37A	121.7	113.5	118.8	100.4	101.7	96.0	24.9	21.6
A36 E70	В	115.1	117.5	110.0	98.7	93.5	92.5	24.8	21.7
	С	115.3	119.0	110.0	99.6	88.5	95.2	24.8	21.4
Average	-	114.0	116.7	112.6	99.6	94.6	94.6	24.2	21.0
Av. E.W.		115	.3	101	.1	94	.6	2:	2.9
	T47A	124.2	125.0	118.5	113.3	85.5	101.2	26.1	23.8
A441 E70	В	124.0	136.8	115.9	126.5	92.0	103.2	26.6	25.2
	C	130.5	134.5	110.6	110.0	97.8	101.0	25.4	24.2
Average		126.2	132.1	115.0	116.6	91.8	101.8	26.0	24.4
Av. E.W.		129	.0	115	.8	96	.8	2.	5.2
	1 57A	126.4	116.0	123.4	98.4	96.8	94.5	24.7	22.6
A514 E70	В	130.8	119.0	121.3	118.0	98.2	92.8	25.5	23.2
	С	129.0	104.1	123.0	92.3	98.3	78.0	27.2	20.3
Average		128.7	113.0	122.6	102.9	97.8	88.4	25.8	22.0
Av. E.W.		120	.8	112	.7	92	2.1		3.9
	T49A	133.0	107.3	124.0	102.2	95.5	99.7	27.2	21.0
A441 E90	B	124.0	110.4	116.4	99.8	94.5	90.8	27.9	20.4
	С	123.6	110.0	115.0	93.8	87.5	87.5	25.7	19.2
Average		126.9	109.1	118.5	98.6	92.5	92.7	26.9	20.3
Av. E.W.		117	.9	102	.6	92	.6	23.4	

*NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

SW K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

4" TRANSVERSE FILLET WELDS

/	SPEC.	ST K/S	5Q. IN.*	Sp K/S	Q. IN.*	SW K/SC	2. IN.*	S K/L	.IN. IN.*
Base-Metal Electrode	23333	East	West	East	West	East	West	East	West
	T59A	126.0	123.8	123.4	115.0	109.5	109.8	29.0	24.2
A514 E90	В	136.0	127.5	119.5	115.7	101.0	95.5	29.2	24.8
	С	125.8	125.0	111.2	122.0	91.8	119.0	28.9	25.6
Average		129.2	125.4	118.0	117.6	100.7	108.1	29.0	24.9
Av. E.W.		127	.3	117	.8	104	.4	20	5.9
	T51A	155.5	156.0	155.5	136.9	124.5	119.5	34.2	28,0
A514 E110	В	159.0	147.5	152.3	136.0	117.3	109.0	35.8	27.2
	С	157.0	133.0	153.7	127.0	112.6	116.0	33.8	27.3
Average		157.2	145.5	153.8	133.3	114.8	114.8	34.6	27.5
Av. E.W.		153	3	143	.0	114	.8	32	2.1
	1,1								
		14.11							
Average									
Av. E.W.					4 1 4				
				7					
					. 7				
Average		17.19							
Av. E.W.				7			1.77		

*NOTES

ST K/Sq. In. - ultimate stress based on measured throat dimension T

Sp K/Sq. In. - ultimate stress based on measured penetration P

SW K/Sq. In. - ultimate stress based on measured fracture width W

SK K/Lin. In. - total failure load divided by total weld length

Photo No. 1

Typical Longitudinal Fillet Weld Specimen As Welded

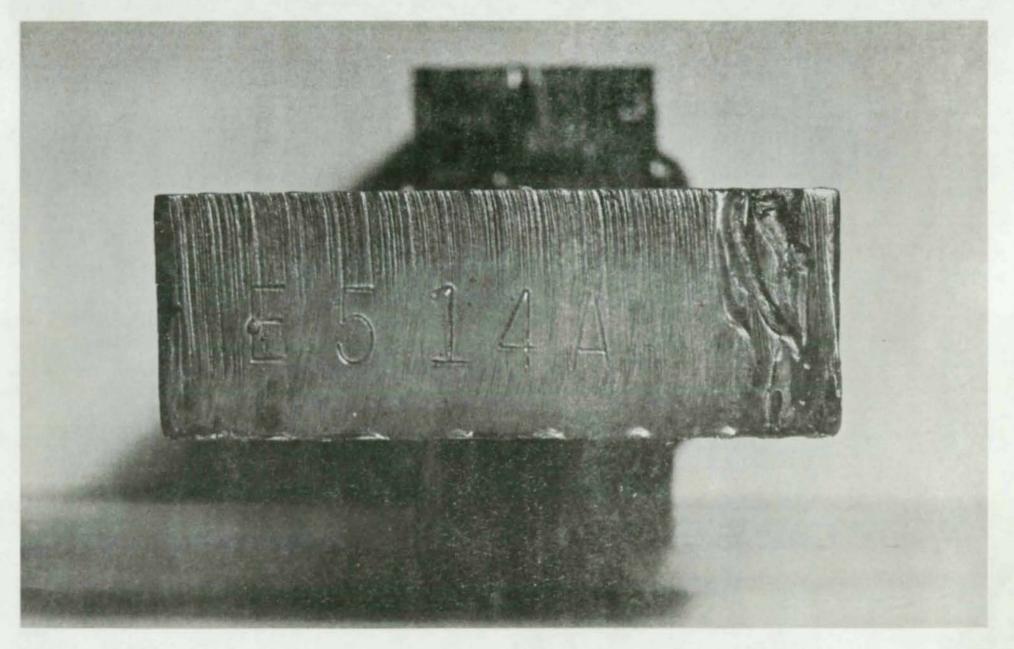


Photo No. 2

Typical Longitudinal Fillet Weld Specimen Showing Identification Mark Stamped On End.



Photo No. 3

Typical Longitudinal fillet weld specimen as machined. Six cuts were made with a bandsaw.

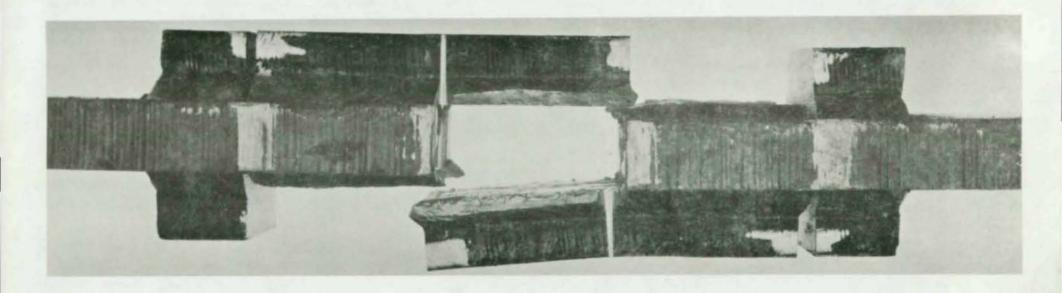


Photo No. 4

Longitudinal fillet weld specimen after testing. This is typical of one of two types of weld fractures.

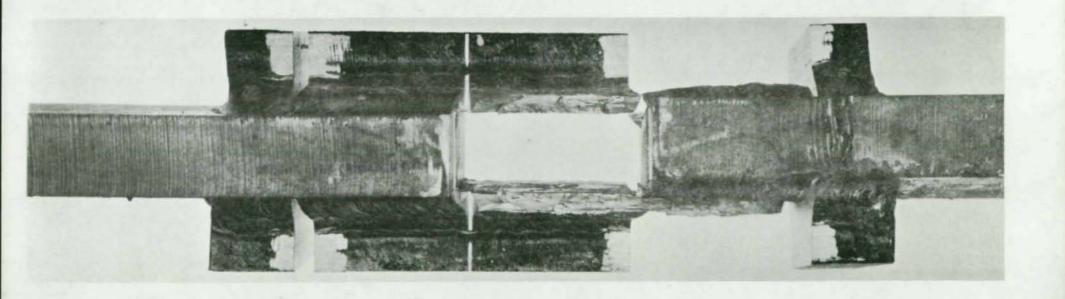


Photo No. 5

Longitudinal fillet weld specimen after testing. This is typical of second of two types of weld fracture that occurred.

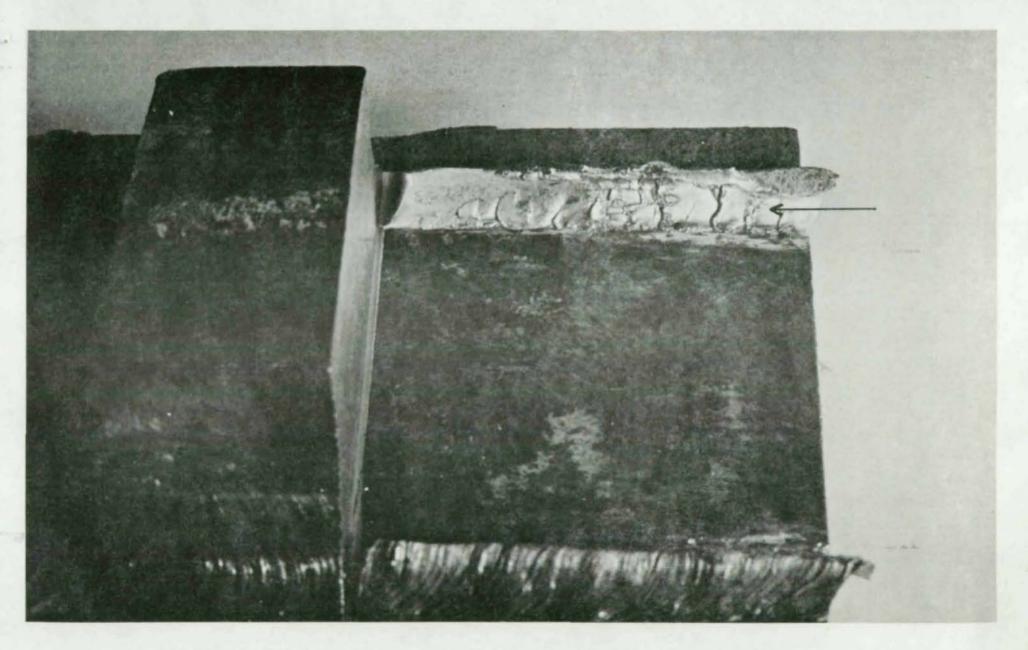


Photo No. 6

Closeup view of longitudinal fillet weld after fracture. The fracture face (arrow) is typical. The width (W) of fracture is average of several measurements across this face.

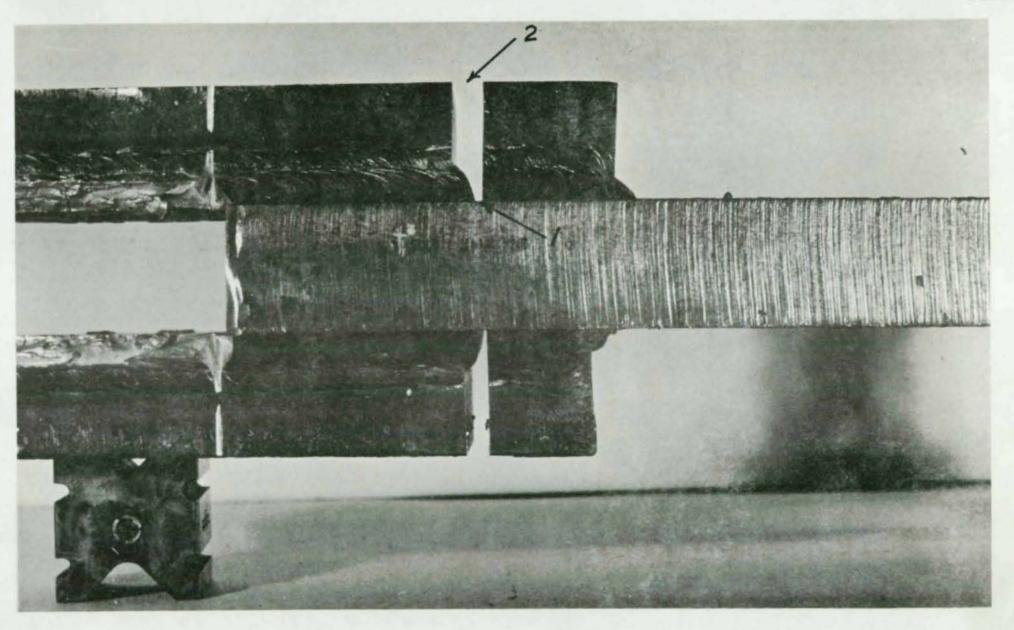


Photo No. 7

Side view of typical longitudinal fillet weld specimen after fracture. Elongation in unfailed weld is shown by difference in notch dimensions. Arrow 1 is original. Arrow 2 is final.

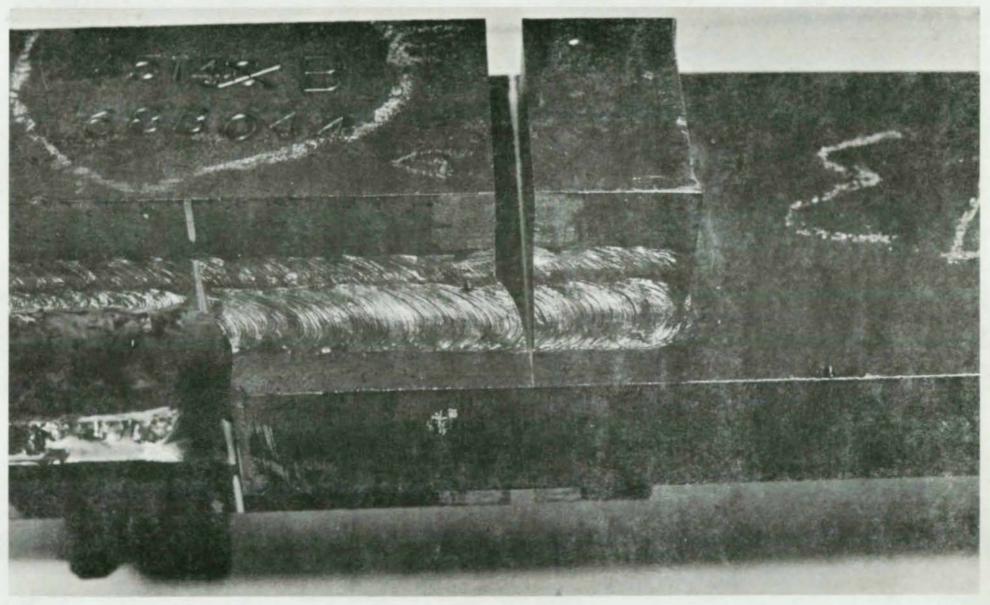


Photo No. 8

Closer view of upper weld in Photo No. 7. Ductility and elongation of weld metal are readily apparent.

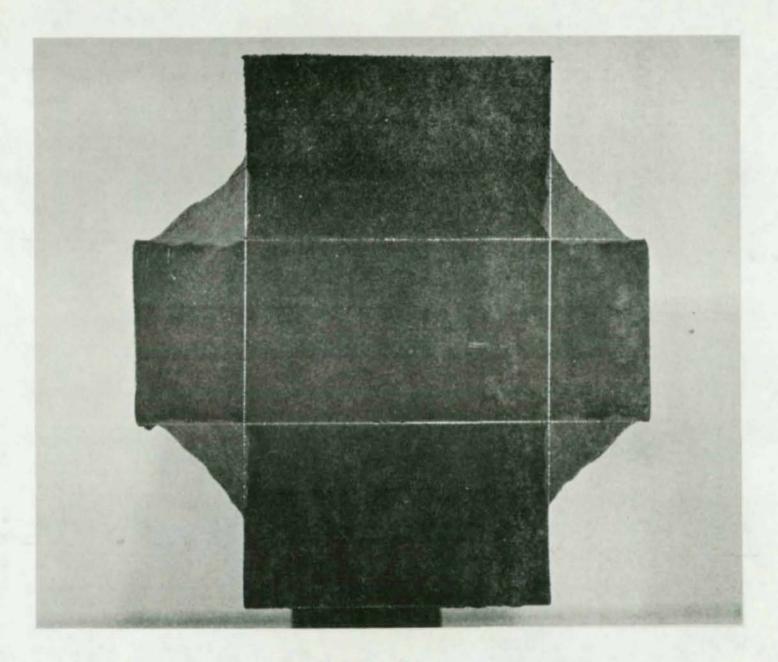


Photo No. 9

Typical macro-etched cross section of unfailed longitudinal fillet weld specimen prepared for measurement of legs, throats and penetration.

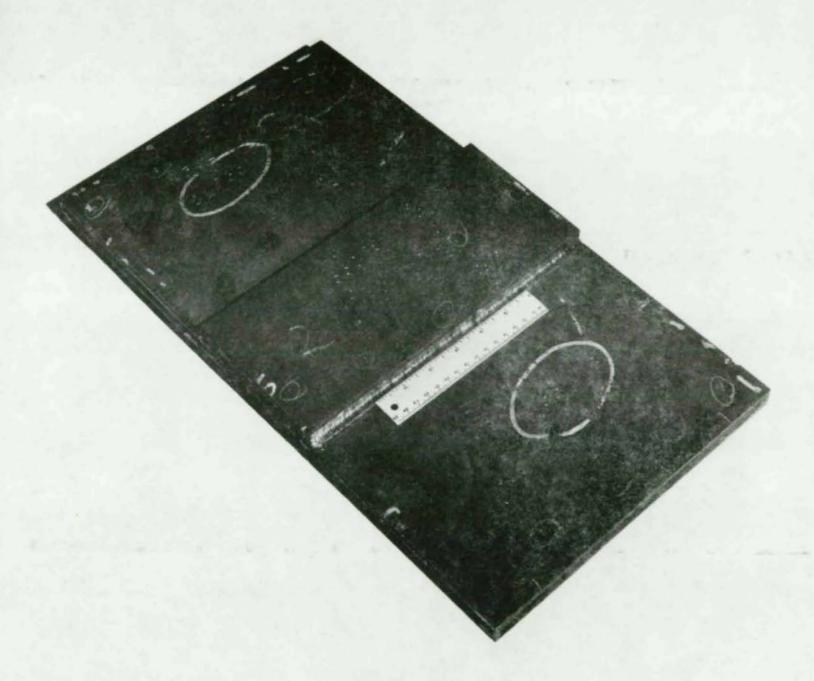


Photo No. 10

Typical transverse fillet weld plate as received. Three test specimens were machined from each plate.

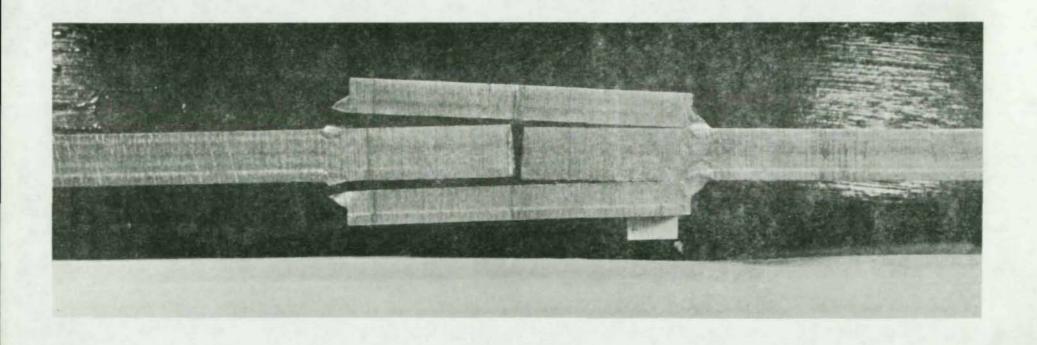


Photo No. 11

Transverse fillet weld specimen after testing. This is typical of one of two types of weld fracture. Note flat angle that weld fracture makes with horizontal.

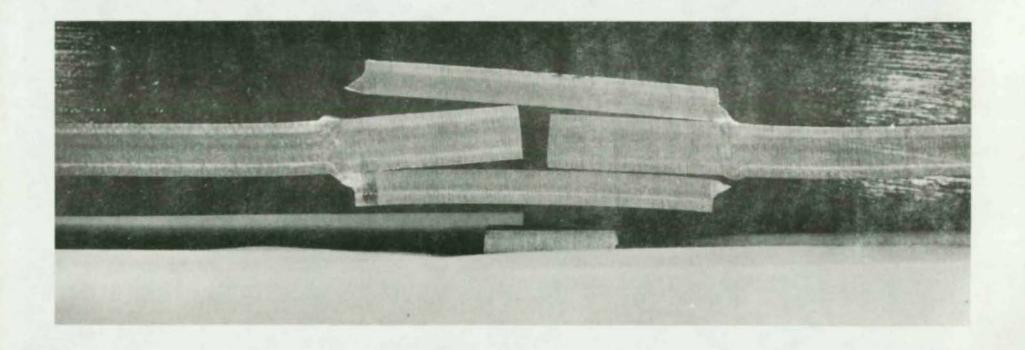


Photo No. 12

Transverse fillet weld specimen after testing. This is typical of second of two types of weld fracture.

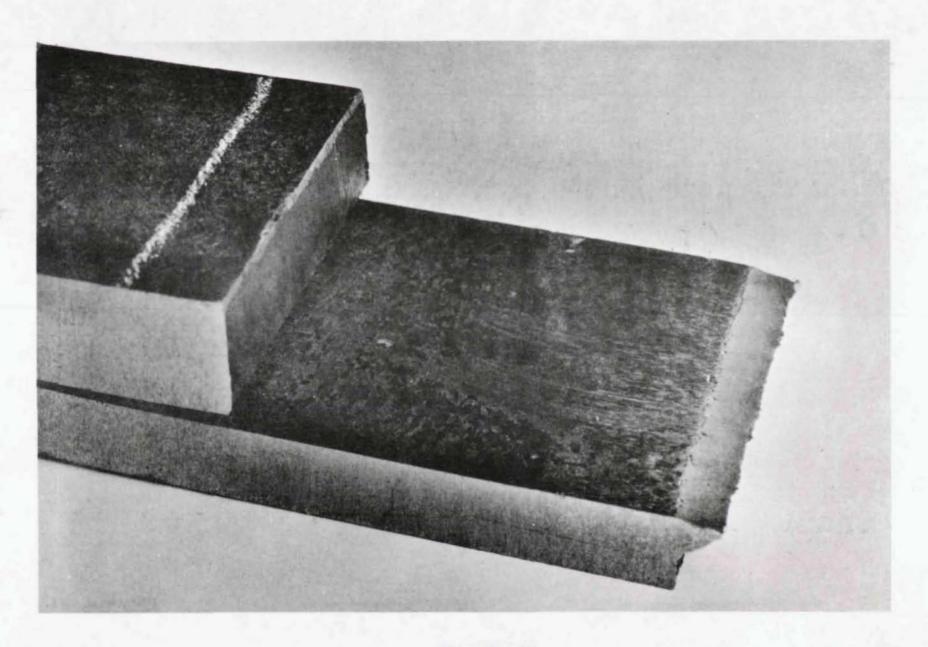


Photo No. 13

Closeup view of typical transverse fillet weld fracture. Fracture face is almost in same plane as base metal.

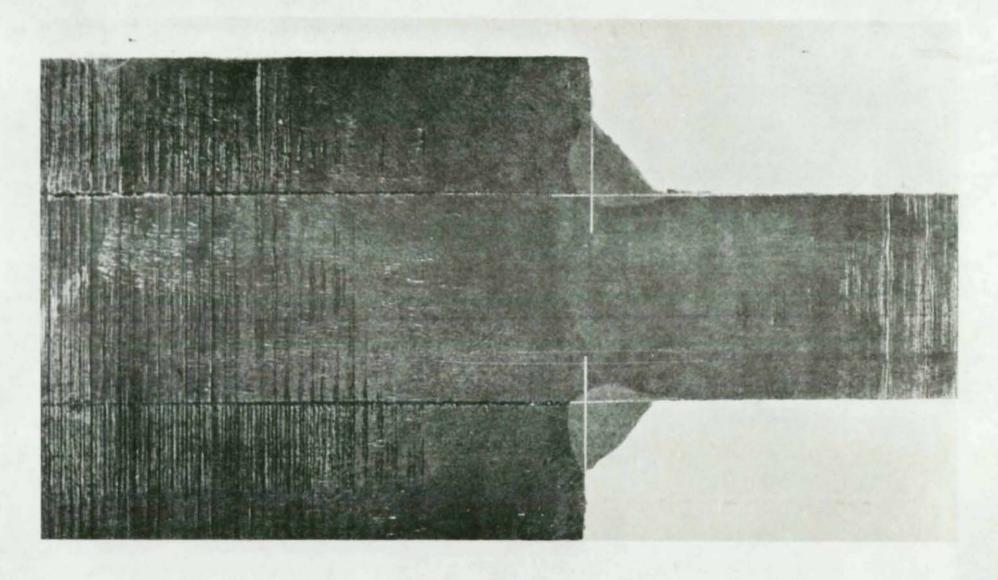
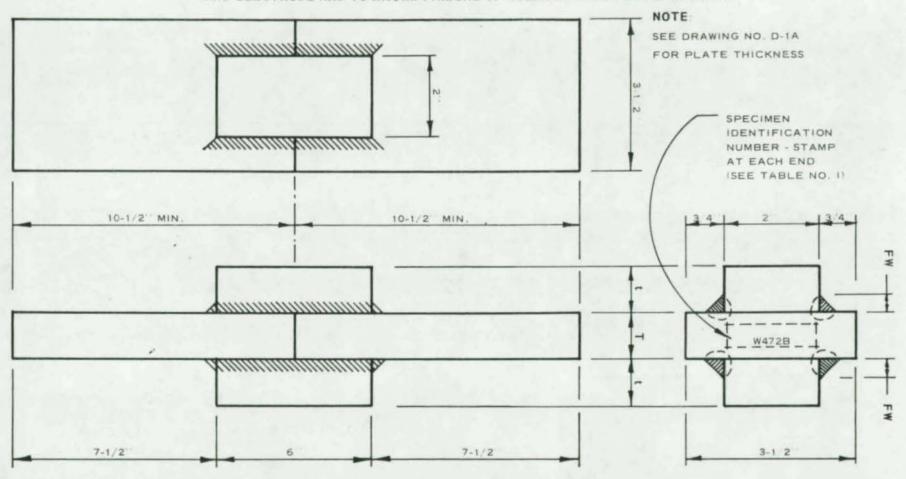


Photo No. 14

Typical macro-etched cross section of unfailed transverse fillet welds prepared for measurement of legs, throat and penetration distance.

PROPOSED LONGITUDINAL FILLET WELD TEST

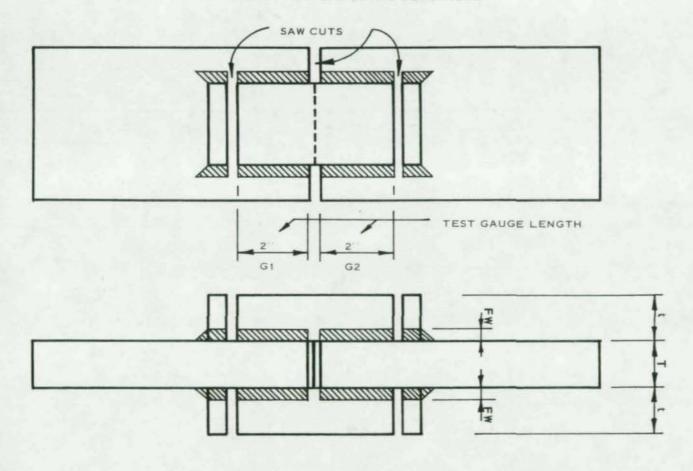
AWS TEST SPECIMEN MODIFIED TO COVER VARIATIONS IN MATERIALS AND ELECTRODE AND TO INSURE FAILURE OF WELDS RATHER THAN BASE METAL



SPECIMEN BLANK
AFTER WELDING - BEFORE MACHINING
DRAWING D - I

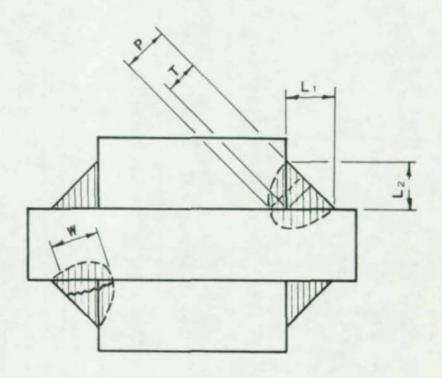
PROPOSED LONGITUDINAL FILLET WELD TEST

AWS TEST SPECIMEN MODIFIED TO COVER VARIATIONS IN MATERIALS AND ELECTRODE



SPECIMEN BLANK AFTER MACHINING DRAWING D = 2

DIMENSION SCHEDULE	DULE		
WELD SIZE - FW	1/4	3 8	1 2
MAIN PLATE THICKNESS - T	3/4	1	1-1 4
SPLICE PLATES THICKNESS - T	3/4	1	1-1-4



CROSS SECTION

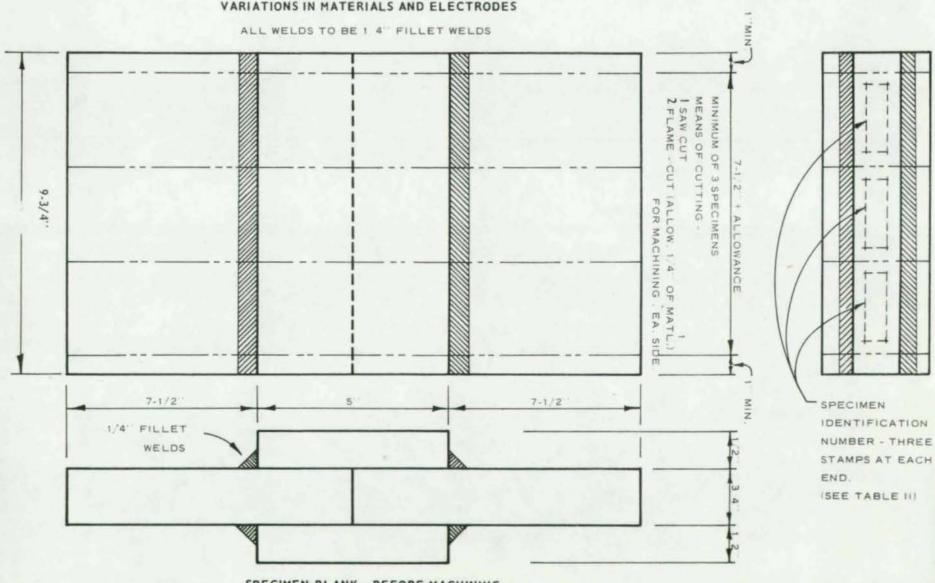
NOTE: CROSS SECTION OF UNFAILED PORTION OF SPECIMEN TO BE CUT AND ETCHED VERTICAL AND HORIZONTAL LINES ARE TO BE SCRIBED CORRESPONDING TO THE ORIGINAL PLATE SURFACES AND THE VERTICAL AND HORIZONTAL LEG SIZES L ARE TO BE MEASURED AND THE MAXIMUM AND MINIMUM VALUES RECORDED ON THE DATA SHEET. THE ACTUAL THROAT T IS ALSO TO BE MEASURED AND RECORDED T IS DEFINED AS THE DISTANCE TO THE FACE OF THE WELD FROM THE INTERSECTION OF THE ORIGINAL PLATE SURFACES W IS DEFINED AS THE AVERAGE WIDTH OF THE FRACTURED SURFACE.

MEASUREMENTS SHALL BE TAKEN WITH A MACHINISTS SCALE TO THE NEAREST HUNDREDTH OF AN INCH.

DRAWING D-3

PROPOSED TRANSVERSE FILLET WELD TEST

AWS TEST SPECIMEN MODIFIED TO COVER VARIATIONS IN MATERIALS AND ELECTRODES

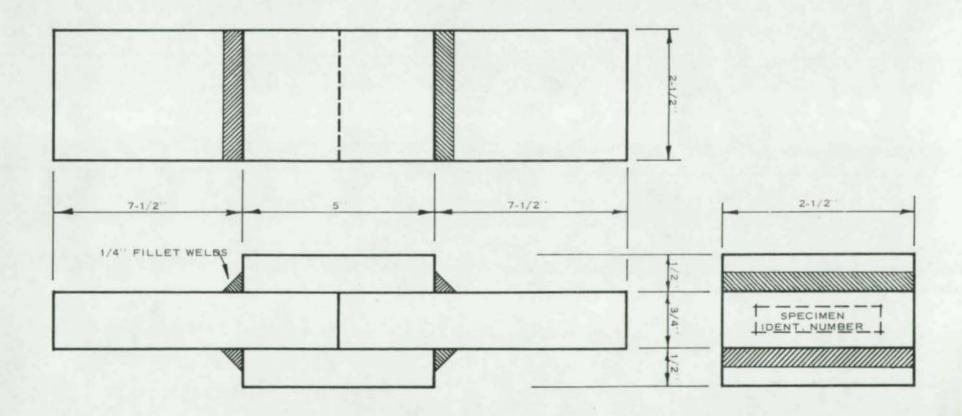


SPECIMEN BLANK - BEFORE MACHINING

DRAWING D - 4

PROPOSED TRANSVERSE FILLET WELD TEST

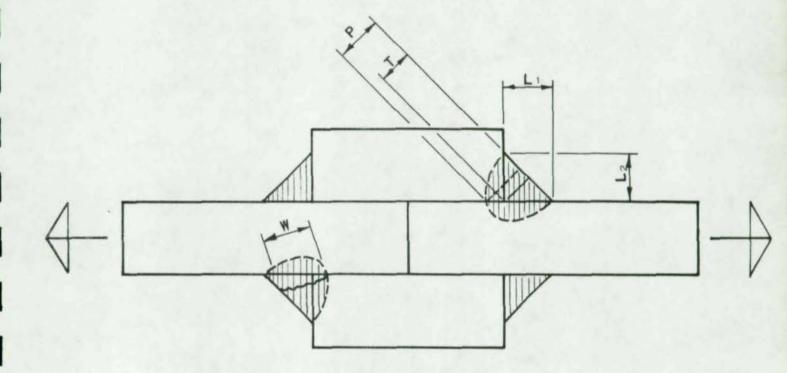
AWS TEST SPECIMEN MODIFIED TO COVER VARIATIONS IN MATERIALS AND ELECTRODES



SPECIMEN BLANK - AFTER MACHINING DRAWING D-5

DRAWING NO. D-6

TRANSVERSE WELD TEST SPECIMEN



CROSS SECTION

NOTE: CROSS SECTION TO BE ETCHED IS MACHINED SIDE ELEVATION OF SPECIMEN.

VERTICAL AND HORIZONTAL LINES ARE TO BE SCRIBED CORRESPONDING

TO THE ORIGINAL PLATE SURFACES AND THE VERTICAL AND HORIZONTAL

LEG SIZES. "L" ARE TO BE MEASURED AND THE MAXIMUM AND MINIMUM

VALUES RECORDED ON THE DATA SHEET. THE "ACTUAL" THROAT, "T" IS

ALSO TO BE MEASURED AND RECORDED. "T" IS DEFINED AS THE DISTANCE

TO THE FACE OF THE WELD FROM THE INTERSECTION OF THE ORIGINAL

PLATE SURFACES. "W" IS DEFINED AS THE AVERAGE WIDTH OF THE

FRACTURED SURFACE. MEASUREMENTS SHALL BE TAKEN WITH A MACHINISTS

SCALE TO THE NEAREST HUNDREDTH OF AN INCH.

TABLE I - SCHEDULE OF MATERIAL AND ELECTRODE COMBINATIONS AND IDENTIFICATION NUMBERS

	ELECTRODE	E-6	012	193	E-70 18			E-90 18			E-11018	
FABRICATOR	BASE SIZE METAL	1/4"	3/8''	1/4"	3/8"	1/2"	1/4"	3/8**	1/2"	1/4"	3/8"	1/2"
		W362A	W363A	W372A	W373A	W374A	W392A					
	A-36	W362B	W363B	W372B	W373B	W374B	W392B		NOTE: N	TEST RE	QUIRED	
		W362C	W363C	W372C	W373C	W374C	W392C					
WEST COAST				W472A	W473A	W474A	W492A	W493A	W494A	W412A		
(W)	A-441			W472B	W473B	W474B	W492B	W493B	W494B	W412B		
				W472C	W473C	W474C	W492C	W493C	W494C	W412C		
				W572A	W573A	W574A	W592A	W593A	W594A	W512A	W513A	W514A
	A-514			W572B	W573B	W574B	W592B	W593B	W594B	W512B	W513B	W514E
				W572C	W573C	W574C	W592C	W593C	W594C	W512C	W513C	W5140
	A-36											
EAST COAST (E)	A-441					ERS ARE T			EXCEPT TH	E		
	A-514											

NOTE - ONLY I SPECIMEN REQUIRED OF EACH IDENTIFICATION NUMBER

IDENTIFICATION NUMBER KEY

1ST DIGIT - FABRICATOR IDENTIFICATION - W' OR E

2ND DIGIT - BASE METAL IDENTIFICATION - 3 = A-36, 4 = A-441, 5 = A-514

3RD DIGIT - ELECTRODE TYPE - 7 = E70 9 = E90 1 = E110

4TH DIGIT - WELD SIZE - 2 = 1 4' , 3 = 3 8' 4 = 1 2

5TH DIGIT - SEQUENCE OF SAMPLE PREPARATION FOR EACH TYPE SPECIMEN - A B & C

SABAB

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	W	KIPS
W362A	1.96	.34	.40	.23	.26	.23	84.5
	1.98	.28	.25	.20	.20	.22	
	2.03	.28	.30	.21	.21	.20	
	2.01	.28	.28	.21	.21	.20	
Average or Total	7.98	.30	.31	.21	.22	.21	
W362B	1.97	.39	.32	.22	.25	.22	84.0
	1.97	.30	.32	.20	.20	.22	
	1.98	.32	.30	.19	.22	.21	
	2.00	.30	.27	.20	.20	.20	
Average or Total	7.92	.33	.30	.20	.22	.21	
w362C	1.96	.31	.31	.19	.22	.16	81.0
	1.91	.32	.27	.21	.21	.21	
	1.94	.35	.33	.23	.25	.22	
	1.96	.29	.28	.20	.20	.21	
Average or Total	7.77	.32	.30	.21	.22	.20	

NOTES: DIMENSIONS GIVEN ARE IN INCHES
SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W

69999

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	w	KIPS
W363A	1.97	.40	.44	.32	.30	.29	122.0
	1.97	.44	.45	,32	.32	.28	
	1.94	.50	.45	.32	.35	.28	
	1.96	.44	.49	.33	.33	.30	
Average or Total	7.84	.45	.46	.32	.33	.29	
W363B	1.94	.50	.50	.33	.33	.29	124.0
	2.00	.52	.54	.35	.35	.30	
	1.98	.49	.51	.32	.32	.28	4,68
	1.99	.43	.49	.30	.30	.29	
Average or Total	7.91	.49	.51	.33	.33	.29	
W363C	2.01	.48	.43	.29	.32	.28	129.0
	2.00	.43	.43	.30	.30	.30	377
	2.02	.43	.44	.30	.31	.31	1
	2.02	.45	.46	.30	,33	.32	
Average or Total	8.05	.45	.44	.30	.32	.30	

NOTES: DIMENSIONS GIVEN ARE IN INCHES
SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L, P, T & W



DATA SHEET - LONGITUDINAL FILLET WELDS

A34 E10

SPECIMEN NO.	GAUGE LENGTH	Li	L 2	Р	Т	W	KIPS
W372A	1.99	.31	.34	.22	.22	.23	118.0
	2.00	. 30	.34	.24	.23	.21	
	2.04	.31	.32	.22	.23	.22	
	2.01	.30	.34	.22	.22	.23	
Average or Total	8.04	.31	.34	.23	.23	.22	
W372B	1.97	.34	.33	.22	.22	.23	114.0
	1.97	.32	.29	.21	.21	.22	
	1.94	.31	.33	.23	.23	.23	
	1.96	.30	.35	.23	.23	.24	
Average or Total	7.84	.32	.33	.22	.22	.23	
W372C	1.92	.29	.33	.23	.23	.23	116.5
	1.97	.30	.30	.22	.22	.23	
	2.00	.30	.31	.22	.22	.24	
	1.99	.32	.33	.22	.22	.22	
Average or Total	7.88	.30	.32	.22	.22	.23	100

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W

1/888

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Lt	L2	Р	Т	W	KIPS
W373A	2.00	.43	.44	.29	.31	.28	147.0
	1.97	.42	.42	.30	,30	.27	0.774
	2.03	.46	.44	.30	.33	.28	
	2.01	.45	.49	.33	.33	.34	
Average or Total	8.01	.44	.45	.31	.32	.29	
W373B	1.98	.50	.47	.29	.31	.29	150.0
	2.00	.57	.43	.30	.30	.29	
	1.99	.51	.44	.27	.30	.28	
	1.99	.47	.46	.27	.29	.29	
Average or Total	7.96	.51	.45	.28	.30	.29	
W373C	2.00	.45	.47	.32	.32	.29	151.0
	2.01	.45	.43	.29	.29	.28	
	1.97	.44	.45	.31	.31	.28	
	2.01	.43	.45	.31	.31	.28	
Average or Total	7.99	.44	.45	.31	.31	.28	

NOTES: DIMENSIONS GIVEN ARE IN INCHES
SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W



DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	P	Т	*	KIPS
W374A	1.96	.47	.54	.36	.36	.38	182.5
1633.30	1.93	.55	.57	.40	.40	.38	
	1.96	.53	.58	.40	.40	.39	
	1.95	.53	.55	.38	.38	~.39	
Average or Total	7.80	.52	.56	.39	.39	.39	
W374B	2,00	.64	.62	.39	.39	.37	187.0
	2.01	.56	.61	.38	.39	.38	
	1.99	.63	.55	.37	.37	.36	
	1.99	.54	.65	.39	.39	.39	
Average or Total	7.99	.59	.61	.38	.39	.38	
w374C	1.98	.62	.49	.38	.38	.38	187.0
	2.01	.54	.58	.39	.39	.36	
	2.01	.53	.52	.37	.37	.37	
	2.00	.58	.55	.39	.42	.40	
Average or Total	8.00	.57	.53	.38	.39	.38	

NOTES: DIMENSIONS GIVEN ARE IN INCHES
SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W



DATA SHEET - LONGITUDINAL FILLET WELDS

A36 E90

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	. w	KIPS
w392A	1.95	.31	.34	.21	.23	.25	117.5
	1.98	.32	.33	.23	.23	.23	
3 1 1 5	1.97	.34	.33	.23	.23	.19	
	1.95	.33	.32	.22	.23	.20	
Average or Total	7.85	.33	.33	.22	.23	.22	
W392B	2.00	.35	.35	.21	.22	.20	129.5
	1.99	.33	.34	.20	.19	.22	
	1.93	.33	.33	,22	.22	.24	
	1.98	.31	.31	.18	.20	.22	
Average or Total	7.90	.33	.33	.20	.21	.22	
W392C	2.02	.33	.33	.22	.23	.22	125.0
	1.98	.36	.36	.20	.25	.23	
	1.93	.30	.31	.23	.23	.23	
	1.99	.32	.37	.21	.23	.22	
Average or Total	7.92	.33	.34	.22	.24	.23	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	т	W	KIPS
W472A	1.97	.31	.31	.26	.24	.22	117.0
	2.00	.31	.35	.26	.26	.21	
all grand	2.01	.32	.30	.24	.24	.22	
	2.03	.31	.34	.27	.27	.21	
Average or Total	8.01	.31	.33	.26	.25	.22	
W472B	1.96	.33	.31	.23	.23	.22	111.0
	1.98	.34	.33	.23	.23	.19	
	2.04	.33	.32	.23	.23	.20	
	2.00	.32	.30	.22	.22	.21	
Average or Total	7.98	.33	.32	.23	.23	.21	
W472C	1.98	.30	.32	.23	.23	.21	115.0
	2,01	.30	.30	.22	.23	.23	
	1.98	.30	.34	.22	.23	.24	
	2.00	.32	.32	.25	.22	.23	
Average or Total	7.97	.31	.32	.23	.23	.23	

JABBB.

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L 2	Р	Т	w	KIPS
W473A	1.96	.47	.44	.32	.32	.30	153.0
	1.97	.43	.43	.28	.31	.28	
	2.02	.42	.38	.28	.28	.31	
	1.98	.43	.43	.30	.30	.31	
Average or Total	7,93	.44	.42	.30	.30	,30	
W473B	2,03	.51	.43	.30	.33	.28	149.0
	2.04	.40	.43	.30	.30	.32	
	2.02	.46	.49	.32	.33	.31	
	2,00	.42	.43	.28	.26	.28	
Average or Total	8.09	.45	.45.	.30	.31	.30	
w473C	1.98	.47	.44	.31	.31	.30	147.5
	1,97	.49	.50	.32	.35	.28	
	1.98	.45	.43	.30	.30	.30	
	1.97	.49	.50	.32	.35	.33	
Average or Total	7.90	.48	.47	.31	.33	.30	

97866

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	W	KIPS
W474A	1.98	.60	.60	.35	.38	.33	169.0
	1.97	.56	.65	.42	.42	.36	
	2.00	.56	.56	.36	.36	.32	
	2.00	. 54	.61	.39	.39	.34	
Average or Total	7.95	.56	.60	.38	.39	.34	
W474B	1.95	.55	.57	.40	.37	.35	172.5
7. 6. 9. 1	1.99	.57	.63	.38	.38	.35	
	1.98	.54	.55	.37	.37	.32	
Stan I	1.99	.55	.62	.37	.37	.31	
Average or Total	7.91	.55	.59	.38	.37	.33	
W474C	1.98	.64	.46	.35	.37	.33	169.0
	1.98	.53	.48	.35	.35	.33	
	1.99	.55	.49	.37	.37	.35	
	1.97	.61	.48	.35	.37	.32	
Average or Total	7.92	.58	.48	.36	.37	.33	



144 E90

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	W	KIPS
W492A	1.98	.32	. 29	.22	.22	.19	104.0
	2.03	.24	.27	.18	.18	.17	
	1.98	.37	.31	.22	.24	.22	
	1.97	.23	.28	.18	.18	.20	
Average or Total	7.96	.29	.29	.20	.21	.20	
W492B	2.01	.31	.28	.21	.21	.20	116.0
	2.03	.27	.28	.20	.20	.20	E CONTRACTOR OF THE PARTY OF TH
	1.96	.33	.31	.22	.22	.18	Liberty.
	1.96	.27	.32	.22	.21	.20	
Average or Total	7.96	.30	.30	.21	.21	.20	
W492C	1,98	.30	.30	.22	.22	.19	112.5
	1.96	.30	.28	.21	.21	.20	
	2.01	.28	.28	.21	.21	.20	
	1.99	,30	.31	.20	.22	.22	
Average or Total	7.94	.30	.29	.21	. 22	.20	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	*	KIPS
W493A	1.96	.42	.45	.30	.30	.28	168.5
	1.97	.44	.46	.31	.32	.29	
	2.02	.40	.45	.30	.30	.30	
	1.99	.50	.46	.31	.33	.30	
Average or Total	7.94	.44	.46	.31	.31	.29	
W493B	1,97	.48	.42	.32	.32	,29	178.0
	1.96	.43	44	28	31	,30	
	1.98	.43	.44	.32	.30	.30	
	1,98	.45	.47	,31	,33	.31	
Average or Total	7.89	.45	.44	.31	.31	:30	
W493C	2.01	.40	.42	.29	.29	.27	165.0
	1.96	.45	.44	.31	.31	.29	
	1.98	.37	.38	.26	.26	.29	
a Same	2.00	.42	.43	.30	.30	.31	
Average or Total	7.95	.41	.42	.29	.29	.29	

6/888

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Lı	L2	Р	Т	W	KIPS
W494A	1.98	.52	.50	.37	.37	.38	199.0
	1.97	.58	.49	.35	.36	.32	
As 11	1.97	.59	.49	.36	.37	.34	Total .
CAMPAGE	2.01	.61	.53	.40	.40	.38	
Average or Total	7.93	.58	.50	.37	.38	.36	
W494B	1.97	.54	,50	.37	.37	.37	196,5
	1.96	.58	.51	.37	.37	.37	
	2.00	.57	.57	.40	.40	.33	
	2,00	.49	.43	.33	.33	.32	
Average or Total	7.93	.54	.50	.37	.37	.35	
W494C	1.98	.57	.48	.37	.37	.37	191.5
	1.98	.64	.48	.37	.37	.35	
	1.95	.53	.56	.40	.40	.35	
72 13 1 2 1 C	1.96	.63	.48	.38	.38	.33	
Average or Total	7.87	.59	.50	.38	.38	.35	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Lı	L2	Р	Т	W	KIPS
W412A	2,00	.28	.30	.20	.20	.18	100.5
	2.02	.27	.28	.18	.20	.19	<u>cadi</u>
	2.05	.25	.26	.18	.18	.20	B
	2.02	.28	.29	.20	.20	.20	
Average or Total	8.09	.27	.28	.19	.20	.19	
W412B	1.94	.28	.30	.16	.20	.21	115.5
	1.95	.32	.33	.24	.23	.19	
	1.97	.32	. 27	.18	.20	.21	
	1.99	.30	.32	.18	.22	.22	
Average or Total	7.85	.31	.31	.19	.21	.21	
W412C	1.95	.32	.30	.20	.22	.19	122.0
	2.00	.25	.29	.19	.19	.20	
	2.02	.27	.27	. 19	.19	.20	
	1.99	.28	.31	.20	.20	.20	
Average or Total	7.96	.28	.29	.20	.20	.20	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	w	KIPS
W572A	1.98	.25	.25	.16	.18	.18	102.0
	1.99	.27	.27	.19	.20	.20	
	1.99	.27	.25	.18	.17	.20	
	2.00	.25	.22	.18	.18	.21	
Average or Total	7.96	.26	.25	.18	.18	.20	
w572B	2.06	.31	.31	.22	.22	.19	105.0
	2.05	.25	.27	.18	.18	.20	
	1,98	.28	.27	.19	.19	.19	
	1,99	.25	.28	.19	.19	.23	
Average or Total	8.08	.27	.28	.20	.20	.20	
w572C	1.96	.26	.24	.16	.18	.20	101.0
	1.98	.26	. 24	.16	.16	.19	
	1.97	.27	.30	.19	.20	.18	Mary Str.
Mile Very	2.00	.27	.26	.17	.19	.20	
Average or Total	7.91	.27	.26	.17	.18	.19	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L, P, T & W

28989

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	w	KIPS
W 573A	1.97	.43	.43	.32	,30	.31	151.0
	2.01	.43	.46	.29	.32	.28	
	1.95	.47	.45	.30	.32	.28	
	1.96	.39	.44	.30	.30	.28	
Average or Total	7.89	.43	.45	.30	.31	.29	
W573B	2.01	.47	.45	.34	.34	.28	166.0
	1.96	.45	.48	.33	.33	.28	
	1.99	.42	.53	.35	.33	.29	
The second	2.00	.44	.51	.36	.34	.33	
Average or Total	7.96	.45	.49	.35	.34	.30	11-00
W573C	1.99	.48	.42	.32	.32	.30	164.0
	1.98	.46	.44	.35	.35	.30	
	1.97	.45	.53	.34	.34	.28	
	1.94	.44	.46	.35	.34	.31	76/8/01/
Average or Total	7.88	.46	.46	.34	.34	.30	

SPRRR

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	w	KIPS
W574A	1.97	.53	. 64	.38	.38	.31	176.5
	1.94	.55	.49	.33	.33	.29	
	2.02	.62	.50	.35	.36	.33	
	2.01	.51	.55	.33	.33	.31	
Average or Total	7.94	.55	.54	.35	.35	.31	
W574B	2.02	.57	.42	.37	.34	.31	173.5
	1.99	.47	.47	.34	.34	.33	
	2.03	.53	.43	.34	.34	.32	
	1.96	.45	.45	.32	.32	.30	
Average or Total	8.00	.51	.44	.34	.34	.32	
W574C	1.99	.50	.48	.35	.35	.31	179.0
	1.98	.56	.49	.37	.37	,36	
	1.99	.46	.53	.35	.35	.31	
	1.98	.53	.52	.37	.37	.34	
Average or Total	7.94	.51	.51	.36	.36	.33	
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AS14 E90

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	KIPS
W592A	2.01	.28	.28	.18	.19	.19	120.0
GOL 1	2.01	.25	.24	.19	.18	.19	
	2.01	.31	.30	.21	.20	.23	
[7-1 to 104	2.01	.23	.26	.17	.18	.20	
Average or Total	8.04	.27	.27	.19	.19	.20	
W592B	2.01	.25	.26	.18	.18	.18	120.5
	1.99	.32	.26	.22	.20	.20	
	2.00	.30	.28	.20	.20	.20	
	1.97	.34	.30	.22	.22	.19	Literal
Average or Total	7.97	.30	.28	.21	.20	.19	
W592C	1.99	.28	.26	.22	.20	.20	119.0
	1.99	.25	.28	.20	.20	.20	
	1.97	.28	.28	.20	.20	.21	1000
	1.98	.30	.27	20	.20	.22	
Average or Total	7.93	.28	.27	.21	.20	.21	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W

SPARR

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	KIPS
W593A	1.99	.48	.45	.32	.33	.29	179.0
	1.96	.47	.45	.32	.32	.29	
	1.98	.45	.49	.33	.33	. 28	
	1.98	.48	.46	.34	.32	.30	
Average or Total	7.91	.47	.46	.33	.33	.29	
W593B	2.00	.46	.43	.30	.30	.28	178.0
	1.98	.49	.51	.30	.33	.30	
	1.98	.53	.40	.31	.30	.31	
	1.98	.46	.49	.28	,32.	.30	
Average or Total	7.94	.49	.46	,30	.31	,30	
w 5 93C	1.96	.39	.45	.30	.30	.29	181.5
	1.97	.45	.44	.32	.32	.27	
	1.99	.49	.39	.30	.30	.28	
	2.00	.45	.45	.33	.33	.30	
Average or Total	7.92	.45	.43	.31	.31	.29	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	P	Т	w	KIPS
W594A	2.01	.53	.57	.36	.36	.33	200.0
	2.00	.55	.58	.36	.36	.34	
	2.00	.50	.51	.32	.31	.32	
	2.03	.50	.60	.34	.34	.31	
Average or Total	8.04	.52	.56	.35	.34	.33	
W594B	2.00	.61	.61	.34	.34	.31	199.0
	1.95	.59	.56	.33	.34	.34	
	1.97	.52	.59	.35	.35	.33	- 46
	1.93	.56	.58	.36	.37	.33	
Average or Total	7.85	.57	. 58	.35	.35	.33	
W594C	1.97	.55	.45	.33	.34	.33	199.0
	1.95	.59	.48	.36	.36	.33	Densit 1
13834139	1.95	.53	.51	.36	.36	.38	
	1.98	.49	.47	.33	.33	.34	
Average or Total	7.85	.54	.48	.35	.35	.35	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	KIPS
W512A	1.98	.30	.27	.18	.18.	.20	125.5
	2.01	.23	.28	.18	.18	.18	
	2.01	.28	.28	.20	.20	.28	
	2.01	.28	.29	.20	.20	.20	
Average or Total	8.01	.27	.28	.19	.19	.22	
W512B	1.96	.26	.29	.19	.19	.19	126.5
	1.94	.25	.27	.18	.19	.21	
	1.97	.27	.27	.17	.18	.19	
	1.99	.25	.28	.17	.19	.18	
Average or Total	7.86	.26	.28	.18	.19	.19	
W512C	1.98	.35	.33	.21	.22	.22	129.5
	2.00	.29	.32	.22	.20	.19	
	1.99	.29	.29	.20	.20	.20	
	2.01	.26	.26	.19	.19	.19	
Average or Total	7.98	.30	.30	.21	.20	.20	

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	KIPS
W513A	1.88	.48	.45	.29	.31	.29	170.0
	1.89	.47	.43	. 28	.30	.34	<u> </u>
THE STATE OF THE S	1.89	.50	.40	. 29	.29	.30	
	1.92	.49	.46	.30	.31	.29	1-0-4
Average or Total	7.58	.49	.44	.29	.30	.31	
W513B	1.96	.44	.43	.30	.30	.28	190.5
	1.94	.38	.47	.29	.29	.31	
	1.84	.48	.48	.34	.34	.30	
	1.89	.40	.44	.32	.30	.32	
Average or Total	7.63	.43	.46	.31	.31	.30	
W513C	1.98	.41	.48	.32	.32	.31	188.5
	1.94	.47	.42	.30	.30	. 29	
	1.91	.48	.48	.32	.35	.30	
	1.89	.43	.43	.30	.30	.34	
Average or Total	7.72	.45	.45	.31	.32	.31	

SPECIMEN NO.	GAUGE LENGTH	L1	L2	P	Т	W	KIPS
W514A	2.02	.56	.49	.37	.37	.35	229.0
	1.97	.55	.51	.37	.37	.38	
	1.98	.53	.46	.34	.34	.36	
LIZE AT	1.98	.60	.46	.37	.37	.35	
Average or Total	7.95	.56	.48	.36	.36	.36	
W514B	1.99	.57	.52	.38	.38	.39	234.0
	1.99	.52	.48	.35	.35	.40	
	1.95	.55	.48	.35	.35	. 34	
	1.98	.53	.43	.33	.33	.33	
Average or Total	7.91	.54	.48	.35	.35	.37	
W514C	1.98	.60	.43	.37	.37	.38	239.0
	2.00	.57	.43	.35	.35	.32	
	1.99	.53	.50	.34	.34	.35	
	2.00	.50	.55	.33	.36	.37	
Average or Total	7.97	.55	.48	.35	.36	.36	

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	w	KIPS
E362A	1.92	.26	.30	. 24	.20	.27	105.0
	1.92	.23	.36	.22	.18	.26	
	1.97	.25	.29	.24	.20	.28	10.00
	1.99	.25	.28	.24	.21	,30	
Average or Total	7.80	.25	.31	.24	.20	.28	
Е362В	1.89	.29	.26	.23	.20	.27	98.5
	1.85	.23	.28	.20	.18	.24	
	1.94	.32	.33	.23	.23	.25	
	1.94	.25	.26	,21	.17	.24	
Average or Total	7.62	.27	.28	.22	.20	.25	
E362C	1.94	.24	.25	.22	.19	.25	109.0
	1.89	.25	.25	,25	.22	.25	
	1.98	.26	.30	.25	.22	.26	in ite
Callestin 1	2.01	.28	.29	.27	.22	.24	Figure
Average or Total	7.82	.26	.27	.25	.21	.25	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W



SPECIMEN NO.	GAUGE LENGTH	L1	L2	P	т	*	KIPS
E363A	1.94	.40	.45	.30	.30	.34	123.0
	1.95	.49	.42	.28	.28	.32	18-16
	1.90	.37	.45	.28	.29	.37	
	1.94	.39	.40	.28	.28	.29	
Average or Total	7.73	.41	.43	.29	.29	.33	
E363B	1.95	.34	.47	.31	.29	.33	129.0
	1.95	.45	.37	.30	.29	.33	
	2.02	.36	.50	.31	.30	.33	
	1.95.	.39	.41	.31	.30	.32	
Average or Total	7.87	.39	.44	.31	.30	.33	
E363C	1.92	.35	.37	.28	.26	.30	123.0
	1.97	.33	.47	.28	.28	.33	E S IN S
	1.96	.33	.36	.26	.25	.27	
	1.95	.39	.45	.29	.28	.25	
Average or Total	7.80	.35	.41	.28	.27	.29	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	*	KIPS
E372A	1.93	.32	.30	.24	.24	.28	117.0
	1.92	.29	.31	.25	.21	.25	
	1.94	.33	.29	.22	.22	.26	
	1.96	.28	.30	.25	.20	.22	
Average or Total	7.75	.31	.30	.24	.22	.25	
Е372В	1.96	.29	.32	.25	.22	.26	119.0
	1.99	.31	.28	.23	.21	.25	
	1.92	.29	.31	.24	.22	.24	
	1.92	.32	.24	.21	.21	.27	
Average or Total	7.79	.30	.29	.23	.22	,26	
E372C	1.96	.35	.31	.25	.23	.25	110.5
	1.93	.31	.28	.20	.21	.25	
	1.95	.34	.25	.20	.20	.24	
	1.96	.28	.25	.21	.19	.25	
Average or Total	7.80	.32	.27	.22	.21	.25	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W

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DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	w	KIPS
E373A	1.96	.40	.54	.32	.31	.35	159.0
	1.95	.47	.43	.34	.33	.38	
	1.98	.43	.41	.35	.31	.35	
	1.97	.49	.41	.34	.32	.35	
Average or Total	7.86	.45	.45	.34	.32	.36	
Е373В	1.95	.45 ,	.43	.34	.32	.41	155.0
	1.96	.45	.36	.33	.33	.38	
	1.94	.43	.46	.35	.30	.38	
100000000000000000000000000000000000000	1.95	.43	.42	.35	.31	.38	
Average or Total	7.80	.44	.42	.34	.32	.39	
E373C	1.98	.42	.50	.36	.32	.36	163.0
	1.98	.50	.41	.33	.32	.40	
	1.99	.39	.55	.35	.33	.35	
	1.97	.44	.45	.32	.32	.35	
Average or Total	7.92	.44	.48	.34	.32	.37	

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DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	т	w	KIPS
E374A	1.88	.45	.54	.46	.37	.41	183.0
	1.92	.49	.57	.41	.37	.39	
	1.99	.43	.60	.39	.35	.36	
	2.00	.51	.57	.42	.37	.43	
Average or Total	7.79	.47	.57	.42	.37	.40	
E374B	1.98	.49	.57	.45	.37	.39	187.5
	1.96	.45	.46	.39	.32	.42	
The state of the s	1.99	.52	.59	.41	.38	.40	
	1.98	.49	.60	.41	.38	.41	
Average or Total	7.91	.49	.56	.42	.36	.41	
E374C	1.95	.50	.57	.45	.38	.42	191.0
	1.96	.59	.62	.45	.43	.46	
	1.93	.50	.62	.42	.39	.44	
	1.92	.51	.50	.41	.38	.43	
Average or Total	7.76	.52	.58	.43	.40	.44	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	W	KIPS
E392A	1.96	.30	.35	.28	.23	.26	123.0
	2.00	.29	.35	.22	.20	.25	
	1.94	.29	.25	.27	.21	.28	
	1.97	.35	.25	.25	.20	.26	
Average or Total	7.87	.21	.30	.26	.21	.26	
E392B	1.94	.31	.36	.26	.25	.28	131.0
	1.97	.34	.25	.26	.22	.26	
	1.90	.27	.32	.25	.22	.29	
	1.94	.33	. 29	.27	.22	.25	
Average or Total	7.75	.31	.31	.26	. 23	.27	
E392C	1.96	.31	.31	.27	. 24	.26	131.5
	1.97	.31	.27	.24	.21	.25	
	1.96	.31	.25	.21	.21	. 27	
	1.96	.29	.26	.24	.20	.25	
Average or Total	7.85	.31	.27	.24	.22	.26	

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	w	KIPS
E472A	1.95	,30	.29	.22	.22	.26	121.0
	1.98	.29	.30	.22	.21	.26	
	1.94	.29	.28	.21	.20	.25	
	1.94	.26	.28	.24	.20	.26	
Average or Total	7.81	.29	.29	.22	.21	.26	
E472B	1.97	.32	.26	.22	.20	,25	121.0
	1.98	.28	.32	.25	.22	.26	T
	1.98	.32	.23	.20	.19	,23	
	2,01	,32	.30	.23	.22	.28	
Average or Total	7.94	.31	.28	.23	.21	.26	
E472C	1.95	.35	.29	.24	.23	.27	123.5
	1.97	.35	.31	.26	.25	.26	
	1.98	.29	.31	.25	.21	.24	
	1.99	.29	.30	.22	.22	.25	
Average or Total	7.89	.32	.30	.24	.23	.26	



SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	w	KIPS
E473A	1.88	.50	.39	.32	.31	.38	167.0
	1.88	.54	.48	.35	.35	.36	
	1.93	.45	.48	.33	.33	.36	
	1.98	.48	.43	.33	.32	.36	
Average or Total	7.67	.49	.45	.33	.33	.37	
E473B	1.94	.55	.43	.36	.32	.42	167.0
	1.95	.40	.41	.35	.30	.38	
EL .	1.93	.55	.41	.36	.33	.36	
	1.96	.38	.32	.35	.27	.37	
Average or Total	7.78	.47	.39	.36	.31	.38	
E473C	1.96	.41	.50	.36	.32	.36	172.0
	1.95	.46	.40	.35	.32	.37	
	1.94	.40	.50	.36	.32	.37	
	1.91	. 53	.43	.40	.34	.38	
Average or Total	7.76	.45	.46	.37	.33	.37	

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	W	KIPS
E474A	1.97	.47	.57	.41	.37	.43	192.0
	1.97	.54	.56	.42	.39	.42	
	2.00	.52	.58	.42	.38	.37	
	1.98	.46	.55	.42	.36	.42	
Average or Total	7.92	.50	.56	.42	.38	.41	
E474B	1.94	.47	.65	.46	.39	.42	190.0
	1,96	.47	.49	.39	.35	.42	
	1.92	.46	.58	.40	.37	.42	
	1.92	.53	.55	.45	.39	.42	
Average or Total	7.74	.48	.57	.43	.38	.42	
E474C	1.95	.49	.59	.40	.38	.39	185.5
	1.95	.56	.59	.43	.40	.39	
	1.94	.47	.61	.37	.37	.44	
	1.92	.51	.54	.42	.39	.39	
Average or Total	7.76	.51	.58	.41	.39	.40	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	T	W	KIPS
E492A	1.96	.33	.34	.28	. 24	.27	136.5
	1.98	.31	.31	,24	.22	,29	
	1.90	.34	.31	.25	,22	.29	
E AT BELLIA	1.93	.30	.33	.26	,21	.27	
Average or Total	7,77	,32	,32	.26	.22	.28	
E492B	2.00	.31	.31	.27	.23	.26	134.5
	1.97	.33	.27	.25	.21	.26	
	2.02	.28	.30	.25	.21	.27	
	2.00	.30	.32	.26	.23	.27	
Average or Total	7.99	.31	.30	.26	.22	.27	
			1000				
E492C	1.97	.33	.25	.22	.20	.25	129.5
	1.94	.34	.29	.21	.19	.28	
	1.97	.29	.34	.23	.18	.27	
	1.96	.30	.34	.22	.20	.27	
Average or Total	7.84	.32	.31	.22	.19	.27	

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SPECIMEN NO.	GAUGE LENGTH	Li	L2	P	Т	w	KIPS
E493A	1.95	.38	.37	.32	.29	.33	171.5
	1.92	.34	.42	.33	.26	.30	
	1.97	.33	.43	.33	.26	.34	
	1.97	.32	.42	,30	.25	.33	
Average or Total	7.81	.34	.41	,32	,26	,33	
E493B	1.97	.42	.40	.30	.27	.32	171.5
12 4 3 DE 14 DE	1.97	.40	.38	.34	.25	.36	
	1.97	.35	.43	.31	.25	.32	
	1.95	.41	.41	.31	.27	.33	
Average or Total	7,86	.40	.41	.32	.26	.33	
E493C	1.96	.41	.37	.35	.30	.34	168.0
	1.96	.38	.35	,33	.28	.33	
	1.94	.33	.37	.30	.29	.31	-
	1.94	.41	.38	.32	.31	.33	
Average or Total	7.80	.38	.37	,33	.30	.33	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	W	LOAD KIPS
E494A	1.94	.34	.50	.37	.29	.43	199.0
	1.88	.39	.51	.37	.30	.42	
	1.92	.41	.51	.38	.32	.41	
	1.95	.34	.37	.34	.36	.43	
Average or Total	7.69	.37	.47	.37	.32	.42	
E494B	1.97	.46	.46	.40	.34	.44	200.0
	1.95	.39	.43	.38	.30	.42	
	1.97	.49	.45	.42	.33	.41	
	1.93	.36	.50	.37	.31	.43	
Average or Total	7.82	.43	.46	.39	.32	.43	
E494C	1.96	.45	.46	.39	.33	.42	204.5
	1.93	.36	.50	.38	.30	.48	
	1.97	.48	.48	.43	.33	.44	
	1.99	.40	.45	.39	.31	.42	
Average or Total	7.85	,42	.47	.40_	.32	.44	

ZAIRS

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	w	KIPS
E412A	1.93	.29	.28	.24	.21	.28	146.5
	1.92	.32	.30	.25	.23	.25	
	1.94	.34	.30	.24	.23	.26	
	1.93	.28	.36	.26	.24	.28	
Average or Total	7.72	.31	.31	.25	.23	.27	
E412B	1.96	,32	.27	.22	.20	.27	148.0
	1.94	.29	.30	.21	.21	.26	
	2.00	.32	.32	.23	.23	.24	
	1.98	.30	.26	.22	.21	.26	
Average or Total	7.88	.31	.29	.22	.21	.26	
E412C	1.90	.29	.31	.25	.20	.28	150.5
	1.92	.34	,29	.26	.21	.25	
	1.95	.27	.31	.23	.18	,31	
	1.95	.34	.25	.27	.22	.25	
Average or Total	7.72	.31	.29	.25	.20	.27	

NOTES: DIMENSIONS GIVEN ARE IN INCHES

SEE DRAWING D-3 FOR LOCATION OF SYMBOLS L. P. T & W



SPECIMEN NO.	GAUGE LENGTH	Li	L 2	Р	т	w	LOAD
E572A	1.92	.32	.23	.22	.22	.27	124.0
	1.89	.33	.26	.21	.21	.22	
	1.94	.34	.27	.22	.21	.26	
	2.02	.32	.30	.24	.23	.26	
Average or Total	7.77	.33	.27	.22	.22	.25	
E572B	1.97	.32	.30	.23	.22	.25	130.5
	1.93	.29	.26	.22	.19	.25	
	1.93	.34	.26	.20	.20	.26	
	1,92	.32	.28	.22	.21	.25	
Average or Total	7.75	.32	.28	.22	.21	.25	
E572C	1.95	.34	.28	.22	.21	.24	122.0
	1.92	.33	.28	.22	.21	.24	
	1.94	.30	.26	.21	.21	.25	
	1.92	.29	.27	.21	.21	.25	
Average or Total	7.73	.32	.27	.22	.21	.25	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	w	KIPS
E573A	1.93	.36	.36	.26	.26	.34	163.0
	1.96	.35	.36	.28	.25	.32	
	1.98	.35	.33	.27	.25	.29	
	2.01	.36	.40	.30	.26	.32	
Average or Total	7.88	.36	.36	.28	.26	.32	
E573B	1.91	.35	.37	.30	.26	.35	162.5
	1.94	.38	.36	.30	.27	.38	
	2.02	.40	.35	.28	.27	.33	
	1.95	.39	.36	.33	.27	.32	
Average or Total	7.82	.38	.36	.30	.27	.35	
E573C	1.97	.35	.39	.27	.26	.31	163.0
	1.97	.37	.37	.28	.27	.34	
	1.98	.34	,41	.31	.28	.32	
	1.97	.39	.39	.30	.28	.35	
Average or Total	7.89	.36	.39	.29	.27	.33	

CAIRR

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	Р	Т	w	KIPS
E574A	1.95	.52	.56	.38	.38	.36	202.0
	1.94	.47	.55	.40	.37	.36	
	1.96	.44	.57	.36	.36	.40	
Control of the	1.94	.47	.48	.36	.36	.37	
Average or Total	7.79	.48	.54	.38	.37	.37	
E574B	1.95	.40	.58	.35	.33	•37	208.0
	1.95	.45	.52	.40	.36	.38	
	1.97	.49	.59	.40	.37	.38	
	1.98	.46	.58	.40	.36	,36	
Average or Total	7.85	.45	.57	.39	.36	,37	
E574C	1.92	.50	.64	.41	.41	.42	190.0
The state of the s	1.90	.42	.56	.42	.35	.39	
	1.97	.42	.59	.37	.35	.38	
	1.98	.52	.59	.43	.40	.36	
Average or Total	7.77	.47	.60	.41	.38	.39	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	w	KIPS
E592A	1,89	.28	.30	.24	.21	.27	147.0
	1.92	.31	.34	.24	.24	.32	
	1.90	.30	.27	.24	.20	.24	
	1.92	.32	.35	.22	.22	.29	
Average or Total	7.63	.30	.32	.24	.22	.28	
Е592В	1.94	.29	.31	.22	.21	.28	143.0
	1.93	.26	.30	.22	.21	.27	
	1.94	.28	.32	.23	.22	.26	
	1.96	.24	.26	.22	.18	.30	
Average or Total	7.77	.27	.30	.22	.21	.28	
E592C	1.97	.35	.34	.24	.24	.26	148.0
	1.94	.26	.27	.23	.20	.26	
	1.95	.33	.28	.23	.21	.26	
	1.94	.35	.30	.26	.23	.27	
Average or Total	7.80	.32	.30	.24	.22	.26	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	p	Т	w	LOAD KIPS
E593A	1.90	.42	.39	.30	.27	.35	182.5
	1.91	.38	.45	.33	.30	.31	
Service March	1.96	.43	.39	.33	.28	.31	
	1.92	.39	.43	.32	.30	.30	
Average or Total	7.69	.41	.42	.32	.29	.32	
E593B	1.94	.39	.39	.31	.27	.36	184.5
	1.90	.38	.43	.28	.28	.33	
	1.97	.41	.36	.30	.28	.35	
	2.00	.41	.41	.34	.28	.29	
Average or Total	7.81	.40	.40	.31	.28	.33	
E593C	2.00	.39	.39	.31	.28	.33	187.5
	2.01	.35	.41	.33	.28	.31	
	1.99	.48	.37	.33	.29	.36	
	1.96	.40	.41	.31	.29	.31	
Average or Total	7.96	.41	.40	.32	.29	.33	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	LI	L2	P	Т	w	KIPS
E594A	1.91	.42	.55	.40	.35	.44	238.0
	1.93	.45	.60	.42	.39	.40	
	1.96	.42	.45	.40	.38	.42	
	1.95	.40	.44	.42	.38	.42	
Average or Total	7.75	.42	.51	.41	.38	.42	
Е594В	1.91	.41	.62	.40	.34	.40	235.0
	1.98	.50	.55	.40	.38	.43	
	1.94	.45	.60	.38	.37	.48	
	1.96	.49	.57	.38	.37	.42	
Average or Total	7.79	.46	.58	,39	.37	.43	
E594C	1.92	.49	.68	.45	.40	.41	237.0
	1.95	.44	.56	.42	.36	.41	
	1.90	.48	.63	.43	.40	.39	
	1.98	,49	.68	,43	.40	.44	
Average or Total	7.75	.48	.64	.43	.39	.41	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	w	KIPS
E512A	1.91	.31	.32	.26	.23	.27	166.0
	1.95	.34	.30	.25	.24	.28	
	1.96	.32	.25	.24	.21	.28	
	1.97	.31	.27	.25	.22	.28	
Average or Total	7.79	.32	.29	.25	.23	,28	
E512B	1,96	.32	.30	.27	,24	.31	163.0
	1.97	.34	.31	.26	.22	.27	
	1.90	.29	.32	.28	.22	.29	
	1.97	.33	.29	.27	.22	.26	
Average or Total	7.80	.32	.31	.27	.23	.28	
E512C	1.98	.29	.29	.25	.21	.26	164.0
	1.94	. 29	.31	.23	. 22	.26	
N. S.	1.96	.29	.28	.21	.21	.27	la l
	1.98	.30	.27	.21	.20	.26	
Average or Total	7.86	.29	.29	.23	.21	.26	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	W	KIPS
E513A	1.94	.34	.44	.30	.28	.34	213.5
	2.00	.38	.39	.30	.28	.34	
	1.91	.30	.40	.30	.26	.34	
	1.92	.37	.38	.30	.27	.41	
Average or Total	7.77	.35	.40	.30	.27	.36	
E513B	1.94	.35	.37	.32	.27	.34	215.5
	1.97	.39	.40	.32	.29	.38	
	1.94	.39	.44	.32	.28	.34	
	1.96	.39	.36	.32	.26	.37	
Average or Total	7.81	.38	.39	.32	.28	,36	
E513C	1.97	.36	.34	.28	.25	.30	212.5
10-	1.95	.34	.34	.28	.25	.33	
	1.92	.38	.40	.27	.27	.30	
White and the	1.97	.43	.35	. 29	.27	.33	
Average or Total	7.81	.38	.36	.28	.26	.32	

DATA SHEET - LONGITUDINAL FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	KIPS
E514A	2.01	.46	.73	.39	.39	.42	274.5
	1.98	.58	.51	.42	.38	.41	
	2,00	.67	.43	.40	.38	.46	
	1.97	,51	.51	.42	.37	.43	
Average or Total	7.96	.56	.54	.41	.38	.43	
E514B	2.00	.52	.65	.41	.41	.45	283.0
	1.96	.49	.55	.41	.38	.44	
	2.01	.49	.70	.41	.40	.43	
	1.98	.51	.55	.41	.39	.39	
Average or Total	7.95	.50	.61	.41	.40	.43	
E514C	1.98	.45	.64	.38	.38	.42	270.0
	1.93	.44	.54	.39	.36	.42	
	1.97	.50	.65	.43	.41	.44	
	1.96	.46	.64	.38	.38	.44	
Average or Total	7.84	.46	.62	.40	.38	.43	0 12

TABLE 2 - TRANSVERSE FILLET WELD TESTS

SCHEDULE OF MATERIAL - ELECTRODE COMBINATIONS AND IDENTIFICATION NUMBERS

ALL WELDS 1/4" FILLET WELDS

	BASE		ELECTRODE	
FABRICATOR	METAL	E70	E90	E110
	A-36	TW37A TW37B TW37C		
WEST COAST (W)	A-441	TW47A TW47B TW47C	TW49A TW49B TW49C	
	A-514	TW57A TW57B TW57C	TW59A TW59B TW59C	TW51A TW51B TW51C
	A-36	TE37A TE37B TE37C		
EAST COAST (E)	A-441	TE47A TE47B TE47C	TE49A TE49B TE49C	
	A-514	TE57A TE57B TE57C	TE59A TE59B TE59C	TE51A TE51B TE51C

IDENTIFICATION NUMBER KEY

IST DIGIT = (T) MEANS TRANSVERSE WELD TEST

2ND DIGIT = FABRICATOR IDENTIFICATION, E OR W

3RD DIGIT = BASE METAL IDENTIFICATION 3 = A-36, 4 = A-441, 5 = A-514

4TH DIGIT - ELECTRODE IDENTIFICATION, 7 = E70, 9 = E90, 1 = E110

5TH DIGIT = SAMPLE NUMBER FOR EACH TYPE OF SPECIMEN

DATA SHEET - TRANSVERSE FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	Li	L2	Р	Т	W	KIPS
TE37A	2.48	.27	.31	.21	.20	. 24	126
	2.57	.29	. 29	.21	.21	.25	
Average or Total	5.05	.28	.30	.21	.205	.245	
TE37B	2,51	.28	.34	. 24	.22	.29	126
	2.58	. 29	.29	.21	.21	.24	
Average or Total	5.09	.285	.315	.225	.215	,265	
TE37C	2.51	.27	.31	.21	.21	.28	124
	2.49	. 28	.34	.24	.22	.28	
Average or Total	5.00	.275	.325	.225	.215	.28	
TE47A	2.55	.27	.33	.22	.21	.31	133
	2.55	.31	.30	.22	.21	.30	
Average or Total	5.10	.29	.315	.22	.21	.305	
TE47B	2.55	.32	.30	.22	.22	.28	136
	2.55	.31	.30	. 24	.21	.30	
Average or Total	5.10	.315	.30	,23	.215	.29	
TE47C	2.54	.27	.31	.22	.21	.27	130
(14 /et 2 /	2.57	.27	. 24	. 24	.18	.25	
Average or Total	5.11	.27	.275	.23	.195	.26	

DATA SHEET - TRANSVERSE FILLET WELDS

SPECIMEN NO.	GAUGE	Li	L2	Р	Т	W	KIPS
TE57A	2.62	.24	.31	.21	.19	.28	129.5
	2,62	.27	.29	.19	.20	. 23	
Average or Total	5.24	.255	.30	.20	.195	.255	
TE57B	2.56	.27	.30	.21	.20	.28	131
	2.57	.24	.31	.21	.19	.24	
Average or Total	5.13	.255	.305	.21	.195	.26	
TE57C	2.45	.33	.30	.23	.22	.29	133
	2.46	.27	.30	.21	.20	.26	
Average or Total	4.91	.30	.30	.22	.21	275	
TE49A	2.50	.28	.29	.22	.20	.28	136.5
	2.50	.31	.28	.22	.21	. 29	
Average or Total	5.00	.295	.285	.22	.205	.285	
TE49B	2.53	.32	.29	.24	,22	.29	140
	2.48	.31	,33	.24	.23	.30	
Average or Total	5,01	.315	.31	. 24	.225	.295	
TE49C	2.53	.28	.29	.22	.20	.27	128
	2,52	,31	.28	.22	.21	.31	
Average or Total	5.05	.295	.285	.22	.205	. 29	

DATA SHEET - TRANSVERSE FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	KIPS
TE59A	2.55	.32	.31	.24	.22	.23	149
	2.59	.38	.30	.23	. 24	.30	
Average or Total	5.14	.350	.305	.235	.23	.265	
TE59B	2.51	.32	.31	.24	.22	.29	143.5
	2.39	.30	.29	.25	.21	.29	
Average or Total	4.90	,31	.30	.245	.215	.29	
TE59C	2.47	.38	.30	.25	.24	.31	143
	2.47	.32	.31	.27	.22	.32	
Average or Total	4.94	.35	.305	.26	.23	.315	
TE51A	2.65	.27	.33	.20	.21	. 24	184
	2.73	.32	.32	.24.	.23	.31	
Average or Total	5.38	.295	.325	.22	.22	.275	
TE51B	2.52	.29	.33	.23	.22	.30	180
	2.51	.32	.32	. 24	.23	.31	
Average or Total	5:03	.305	:325	:235	.225	•305	
TE51C	2;62	:32	:32	.23	.23	.31	177.5
	2,63	.24	.34	,21	.20	,29	
Average or Total	5.25	.28	.33	.22	.215	.30	

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DATA SHEET - TRANSVERSE FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	LOAD
TW37A	2.51	.27	.27	•20	.18	.21	108250
	2.51	.26	.30	.23	.20	.24	
Average or Total	5.02	.265	.285	.215	.19	.225	
TW37B	2.49	.28	.28	.20	.19	.24	108250
	2.50	.25	.29	.24	.18	.23	
Average or Total	4.99	.265	.285	.22	.185	.235	
TW37C	2.41	.24	.30	.24	.18	.22	103500
	2.42	.31	.21	.19	.18	.23	
Average or Total	4.83	.275	.255	.215	.18	.225	
TW47A	2.42	.23	.26	.21	.17	.22	115250
476	2.43	.28	.28	.21	.21	.25	
Average or Total	4.85	.255	.27	.21	.19	.235	
TW47B	2.52	.25	.26	.19	.18	.25	128000
	2.54	.26	.28	.21	.19	.24	
Average or Total	5.06	.255	.27	.20	.185	.245	
TW47C	2.46	ė 27	. 26	.22	.18	.25	119500
	2.47	.25	.28	,22	.18	.23	
Average or Total	4.93	.26	.27	.22	.18	.24	

DATA SHEET - TRANSVERSE FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L2	Р	Т	W	LOAD
TW57A	2.48	.28	.28	.23	.19	.23	112500
	2.49	.28	.29	.23	.20	.25	
Average or Total	4.97	.28	.285	.23	.195	.24	
TW57B	2.55	.28	.29	.21	.20	.25	119000
	2.58	.27	.26	.22	.19	.25	
Average or Total	5.13	.275	.275	.215	.195	.25	
TW57C	2.51	.28	.28	.22	.20	.29	102000
	2.51	.26	.27	.22	.19	.23	
Average or Total	5.02	.27	.275	.22	.195	.26	
TW49A	2.61	.29	.28	.21	.21	.22	109750
	2,63	.23	.27	.20	.18	.20	
Average or Total	5.24	.26	.275	.205	.195	.21	
TW49B	2.48	.25	.29	.21	.19	.23	102500
	2.48	.23	.27	.20	.18	.22	
Average or Total	4.96	.24	.28	.205	.185	-225	1
TW49C	2.49	.22	.30	.21	.17	.22	95750
	2.49	.23	.27	.20	.18	.22	
Average or Total	4.98	.225	.285	.205	.175	.22	

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DATA SHEET - TRANSVERSE FILLET WELDS

SPECIMEN NO.	GAUGE LENGTH	L1	L 2	Р	Т	W	LOAD
TW59A	2.48	.31	.27	.23	.20	.23	119500
Fig. 1	2.47	.26	.28	.19	.19	.21	
Average or Total	4.95	.285	.275	.21	.195	. 22	
TW59B	2.55	.30	.27	.22	.20	.26	125750
	2.50	.25	.26	.21	.19	.26	
Average or Total	5.05	.275	.265	.215	.195	.26	
TW59C	2.51	.30	.28	.21	.21	.23	128500
	2.50	.24	.27	.21	.20	. 24	
Average or Total	5.01	.27	.275	.21	.205	.235	
TW51A	2.45	.27	.24	.20	.18	.23	137500
	2.45	.26	.25	.21	.18	.24	
Average or Total	4.90	.265	.245	.205	.18	.235	
TW51B	2.47	.27	.250	.19	.18	.25	136000
	2.52	.28	.25	.21	.19	.25	
Average or Total	4,99	.275	.25	.20	.185	.25	
TW51C	2.48	.29	.27	.21	.21	.25	135000
	2.46	.30	.26	.22	.20	.22	
Average or Total	4.94	.295	.265	.215	.205	.235	

JOB

A.W.S. Fillet Weld Study SPECIMEN Base metal used for specimens

A.S.T.M.	HEAT	SIZE	AREA	LOAD IN	POUNDS	LBS, PE	R 5Q. IN.	ELONG	ATION		NATURE OF	BEND TES
Desig.	NUMBER		SQ. IN.	POINT	MAXIMUM	POINT	TENSILE STRENGTH	2 IN	PER CENT	IN/8 IN.	FRACTURE	
A36	PAA66C406	.505 x 1.511	.763	31750	55000	41610	72080	.92	46.0	2.31	Silky	
A36	PAC72C700	.762 x 1.527	1.164	43250	76500	37160	62720	1.18	59.0	2.45	Silky	
A36	PAH70C711	1.017 x 1.506	1.532	56750	105250	37040	68700	.67	33.5	2.34	Silky	
A36	PAN40-450	1.258 x 1.511	1.901	70250	137250	36950	72200	1.08	54.0	2.00	Silky	
A-441	PBA69C471	.493 x 1.509	.744	37500	55750	50400	74930	.93	46.5	1.99	Silky	
A-441	PBC74B131	.749 x 1.568	1.174	65000	96500	55370	82200	.97	48.5	1.95	Si1ky	
A-441	PBH71B264	1.000 x 1.509	1.509	88000	129500	58320	85820	1.07	53.5	1.94	Silky	
A-441	PBM65B677	1.259 x 1.628	2.050	100500	164750	49020	80370	1.15	57.5	2.12	Silky	
A-514	PCA73B886	.506 x 1.551	.785	86000	93250	109550	118790	.62	31.0	1.13	Silky	
A-514	PCC66B008	.768 x 1.391	1.068	107000	117500	100190	11020*	.69	34.5	1.12	Silky	
A-514	(Retest) PCC66B008	.767 x 1.627	1.248	136250	148250	109170	118790	.75	37.5	1.10	Silky	
A-514	PCH71C675	1.016 x 1.433	1,456	165750	179500	113840	123280	.72	36.0	1.23	Silky	

REMARKS: East Coast base metal. * Failure, see retest following. REPORTED TO:

BY Q.H. Kenten

JOB A.W.S. Fillet Weld Study
SPECIMEN Base metal used for specimens

	HEAT	SIZE	AREA	LOAD IN	POUNDS	LBS, PE	R 5Q. IN.	ELONG	ATION	141.4	NATURE OF	BEND TEST
	NUMBER		SQ. IN.	POINT	MAXIMUM	POINT	TENSILE STRENGTH	IN IN	PER CENT	IN/8 IN.	FRACTURE	BENO TEST
-514	PCN73C190	1.279 x 1.454	1.860	194000	236250	104300	127020	.73	36.5	1.07	Silky	
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REMARKS:

East Coast Base Metal

REPORTED TO:

BY R.H. Kenter

JOB

A.I.S.C. Fillet Weld Test SPECIMEN Base metal used for specimens

A.S.T.M.	HEAT	SIZE	AREA	LOAD IN	POUNDS	LBS. PER	9 5Q. IN.	ELONG	ATION		NATURE OF	BEND TEST
Desig.	NUMBER		5Q. IN.	POINT	MAXIMUM	POINT	TENSILE STRENGTH	2 IN	PER CENT	IN/8 IN.	FRACTURE	DENO 123
A-36	8129117	.767 x 1.517	1.164	40500	74500	34790*	64000	1.19	59.5	2.67	Silky	
A-36	8129117	.794 x 1.513	1.201	42500	74250	35390**	61820	.67	33.5	2.68	Silky	
A-36	8247653	1.020 x 1.475	1.505	52750	100500	35050*	66780	1.21	60.5	2.66	Si1ky	
A-36	8247653	1.018 x 1.513	1.540	61250	104500	39770**	67860	.66	33.0	2.64	Silky	
A=36	9906672	1.271 x 1.433	1,821	69250	136500	47370	74960	1.20	60.0	2.40	Silky	
A-36	328859	1.490 x .764	1.138	49100	77500	43150	68100	1.06	53.0	2.30	Si1ky	
A-441	72215	.502 x 1.554	.780	39900	61600	51150	78970	1.00	50.0	2.17	Silky	
A-441	24258	.754 x.1.533	1.156	59000	89750	51040	77640	1.01	50.5	2.09	Silky	
A-441	24258	1.495	1.157	58300	90000	50390	77790	1.00	50.0	2.16	Si1ky	
A-441	96A337	1.030 x 1.453	1.497	72000	117750	48100	78660	1.03	51.5	2.05	Silky	
A-441	97B216	1.288 x 1.534	1.976	105750	164250	53520	83120	.98	49.0	1.98	Silky	
A-514	66C281	.520 x.1.498	.779	78250	84500	100450	108470*	.63	31.5	1.07	Silky	

REMARKS: West Coast base metal.

REPORTED TO:

BY R. H. Kersten

JOB SPECIMEN A.I.S.C. Fillet Weld Test Base metal used for specimens

A.S.T.M. Desig.	HEAT	SIZE	AREA SQ. IN.	LOAD IN POUNDS		LBS, PER SQ. IN.		ELONGATION			NATURE OF	BEND TEST
				POINT	MAXIMUM	POINT	TENSILE STRENGTH	2 '*	PER CENT	IN/s IN.	FRACTURE	BEND TEST
A-514	81P337	.780 x 1.544	1.204	131500	141250	109220	117320	.60	30.0	1.00	Silky	
1-514	738665	× 1.535	1.141	131000	141250	114810	123790	.64	32.0	1.01	Silky	
A-514	60B044	1.019 x 1.435	1.462	157000	171000	107390	116960	.69	34.5	1.03	Silky	
A-514	99₽795	1.263 x 1.493	1.886	233250	250000	123670	132560	.61	30.5	.96	Silky	
A-514	66C281	.518 x 1.513	.784	80200	86600	102300	110450*	* .65	32.5	1.15	Silky	
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REMARKS: West

* Failure

REPORTED TO:

** Retest

BY R. H. Kersten

