The following list represents corrections to the first printing of AISC Design Guide 13, Stiffening of Wide-Flange Columns at Moment Connections: Wind and Seismic Applications.

Page(s) | Item
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9 | In the left column, the definition for \( \alpha_m \):
\[
\alpha_m = 1.36 \left( \frac{P_e}{d_b} \right)^{1/4}
\]
for a four-bolt unstiffened extended end plate
\[
= 1.13 \left( \frac{P_e}{d_b} \right)^{1/4}
\]
for an eight-bolt stiffened extended end plate
should be replaced with:
\[
\alpha_m = 1.36 \left( \frac{P_e}{d_b} \right)^{1/4}
\]
9 | In the left column, the definition for \( k_i \) should be replaced with, “distance along the column flange from the center of the column web to the toe of the fillet, in.”
32 | In the left column, Equation 4.4-7 should read:
\[
w_{min} = \frac{0.9 \times 0.6 F_y t_{eff}}{0.75 \times 0.6 F_{EXX}} (\sqrt{2})
= \frac{1.70 F_y t_{eff}}{F_{EXX}} \geq t_{eff} \sqrt{2}
\]
41 | At the top of the right column, the minimum web doubler plate thickness, \( t_{p, min} \), should be replaced with:
\[
t_{p, min} = \frac{h \sqrt{F_y}}{418} \left[ \frac{13.9 \text{ in.} - 2(1.25 \text{ in.})}{36 \text{ ksi}} \right]
= 0.164 \text{ in.}
\]
52 | In Example 6-7 at the top of the left column, lines 2 through 8 should be replaced with:
\[
N = t_f + 2w + 2t_p = 0.507 \text{ in.} + 2(1/2 \text{ in.}) + 2(3/4 \text{ in.}) = 3.01 \text{ in.}
\]
\[
N_d = \frac{3N}{d_e} = \frac{3(3.01 \text{ in.})}{13.9 \text{ in.}} = 0.650
\]
\[ \phi R_u = 0.75 \times 135 C t_w^2 \times \left[ 1 + N_k \left( \frac{t_w}{t_f} \right)^{1.5} \right] \times \sqrt{\frac{F_{yf} t_f}{t_w}} \]

\[ = 0.75 \times 135(1)(0.370 \text{ in.})^2 \times \left[ 1 + (0.650) \left( \frac{0.370 \text{ in.}}{0.660 \text{ in.}} \right)^{1.5} \right] \times \sqrt{\frac{(50 \text{ ksi})(0.660 \text{ in.})}{0.370 \text{ in.}}} \]

\[ = 167 \text{ kips} \leq P_{nf} = 172 \text{ kips} \quad \text{n.g.} \]