

Revision and Errata List—July 2020
AISC *Seismic Design Manual*, 3rd Edition

The following list represents corrections to the First Printing of the AISC *Seismic Design Manual*, 3rd Edition. These corrections are incorporated in the Second Printing dated January 2020.

Page(s)	Item
viii	Insert the following after the 1 st sentence in the Scope section: Other structures are defined as structures designed, fabricated, and erected in a manner similar to buildings, with building-like vertical and lateral load resisting elements.
3-32	In the ASD column at the top half of the page, revise ϕR_n to $\frac{R_n}{\Omega}$.
4-43	Revise the sentence near the bottom of the page to say, “The seismic design story drift between the second...”
4-113	Near the middle of the page, revise calculation result to, “= 480 kips < 691 kips.” At the last line of calculations, revise to, “= 479 kips < 691 kips n.g. ”
4-133	Revise the panel zone strength calculations as follows: $\alpha P_r = 1.0(249 \text{ kips})$ $= 249 \text{ kips}$ $0.75 P_y = 0.75 F_y A_g$ $= 0.75(50 \text{ ksi})(51.8 \text{ in.}^2)$ $= 1,940 \text{ kips}$ For $\alpha P_r \leq 0.75 P_y$, the design strength of the panel zone is given by AISC <i>Specification</i> Equation J10-11.
4-142	In the first paragraph, revise $(P_{rc} < 0.3 P_r)$ to $(P_{rc} < 0.3 P_c)$.

4-220

Revise the required plate washer load and flexural strength as follows:

LRFD	ASD
For the plate washer load, w_u : $w_u = \frac{N_{ua}}{4A_{brg}}$ $= \frac{378 \text{ kips}}{4(17.0 \text{ in.}^2)}$ $= 5.56 \text{ ksi}$ For a 1-in. strip of plate: $M_u = \frac{w_u l^2}{2}$ $= \frac{(5.56 \text{ ksi})(1 \text{ in.})(0.500 \text{ in.})^2}{2}$ $= 0.695 \text{ kip-in.} < 11.3 \text{ kip-in.} \quad \mathbf{o.k.}$	For the plate washer load, w_a : $w_a = \frac{N_{aa}}{4A_{brg}}$ $= \frac{268 \text{ kips}}{4(17.0 \text{ in.}^2)}$ $= 3.94 \text{ ksi}$ For a 1-in. strip of plate: $M_a = \frac{w_a l^2}{2}$ $= \frac{(3.94 \text{ ksi})(1 \text{ in.})(0.500 \text{ in.})^2}{2}$ $= 0.493 \text{ kip-in.} < 7.49 \text{ kip-in.} \quad \mathbf{o.k.}$

5-222

After the weld length calculation, the welds noted as 1¼-in. fillet welds should be ¼-in. fillet welds.

9.1-243

Remove the heading “3. Continuity Plate Welding.”

9.1-291

In Fig. C-F3.4, definition of θ_p , replace $\Delta_p h$ with Δ_p/h

9.2-38

In the equation for N , revise b_f to t_{bf} :

$$N = t_{bf} + 2w + 2t_p, \text{ in. (mm)}$$