TOWARD A 100 YEAR BRIDGE COATING SYSTEM: BRIDGE TOPCOATS IN JAPAN



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BIOGRAPHY

Winn Darden is Business Manager for LUMIFLON® fluoropolymer resins for the Americas. He has over 25 years of sales and marketing protective experience in coatings and coating raw materials. Mr. Darden is the author of more than 20 papers presented at meetings of the Society of Protective Coatings (SSPC), the National Association of Corrosion Engineers (NACE), the International Bridge Conference, National Steel Bridge Alliance, and the New York City Bridge Conference among others. He holds a BS in Chemistry and an MBA from the University of Texas at Austin.

SUMMARY

Fluoropolymers have been used as topcoats for bridges in Japan for more than 30 Based on extensive years. laboratory testing and long term results from the field, these materials are now required as topcoats on all bridges in Japan. Properly applied, fluorinated topcoats can increase coating system life to more than 60 years, with a goal of 100 years of topcoat life. These fluoropolymer topcoats offer substantial reductions in life cycle costs compared to conventional coating This paper will systems. discuss test results from both field and laboratory studies demonstrating the long term durability of fluorinated topcoats. Surface preparation application and coating methods used in Japan will be reviewed. Finally, the life cycle cost advantages of fluorinated topcoats will be shown.

TOWARD A 100-YEAR BRIDGE COATING SYSTEM: BRIDGE TOPCOATS IN JAPAN

Abstract

Fluoropolymers have been used as topcoats for bridges in Japan for more than 30 years. Based on extensive laboratory testing and long-term results from the field, these materials are now required as topcoats on all bridges in Japan. Properly applied, fluorinated topcoats can increase coating system life to more than 60 years, with a goal of 100 years of topcoat life. These fluoropolymer topcoats offer substantial reductions in life cycle costs compared to conventional coating systems. This paper will discuss test results from both field and laboratory studies demonstrating the long-term durability of fluorinated topcoats. Surface preparation and coating application methods used in Japan will be reviewed. Finally, the life cycle cost advantages of fluorinated topcoats will be shown.

Keywords: Coating, paint, bridge, maintenance, topcoat, fluoropolymer, fluorourethane, weatherability, durability, life cycle cost.

Introduction

Coatings are used on steel bridges primarily to prevent corrosion and subsequent degradation of structural properties, secondarily for aesthetics. The development and widespread use of zinc rich primers beginning in the 1970's have resulted in substantial improvement of corrosion resistance of the typical bridge coating system. Many bridges using zinc rich primers have been in service for more than 30 years without exhibiting corrosion. The struggle has been to find topcoats, which can match or exceed the longevity offered by zinc rich primers. Over the last 30 years, many longer-lived types of coatings have been used with varying success including polyurethanes and polysiloxanes. While these topcoats offer significant improvement over materials such as alkyds and chlorinated rubber, these topcoats will begin to chalk and fade years before the primers are affected, to the detriment of bridge appearance.

Aesthetics are becoming more important in the bridge market. As cities and communities try to attract residents and businesses, they are requesting the use of attractive colors and designs on infrastructure. Selecting colors like red, blue, and green, using special lighting, and improving landscaping allow repurposing and upgrading of bridge structures⁽¹⁾. Long term gloss and color retention are difficult to achieve with conventional coating systems, meaning that maintenance painting will be required, sometimes after only short periods of time.

Fluoropolymer Coatings

Fluoropolymers have been used in coatings since the mid 1960's, mainly in architectural applications. The best known fluoropolymer coating is polyvinylidene fluoride, or PVDF. Topcoats made with PVDF offer a potential life of around 30 years while maintaining color and gloss. However, PVDF coatings are suitable only for shop application via a coil coating process, where temperatures above 200° C are used to form the coating. This makes them unsuitable for field application, and almost impossible to use in a steel fabrication shop.

A new class of fluoropolymer resins known as FEVE (fluoro ethylene vinyl ether) resins offers characteristics that enable them to be used where PVDF coatings cannot. FEVE resin based coatings can be thought of as hybrids between conventional polyurethane coatings and pure fluoropolymer coatings. Their unique polymer structure allows them to be dissolved in common solvents and to be chemically reacted to form a cross-linked polymer structure like an epoxy or polyurethane. These properties mean that FEVE resins can be used at room temperature to form a hard cross-linked polymer via chemical reaction and solvent evaporation. This makes maintenance painting on site and use in steel fabrication shops possible, since elevated temperatures are not required to form the coating. Because of the fluoropolymer portion of the polymer, FEVE-based coatings offer outstanding weatherability similar to that of PVDF and other properties as discussed below.

Properties of FEVE-Based Fluoropolymer Coatings

FEVE-based fluoropolymer topcoats offer several advantages over conventional coatings, the most important being weatherability and corrosion resistance.

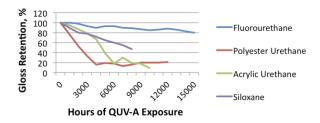
Weatherability of FEVE-Based Fluoropolymer Coatings⁽²⁾

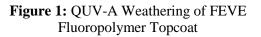
Two types of weathering tests are used for coating systems: accelerated weathering and natural weathering. Both are discussed below.

Accelerated Weathering Test Results

Accelerated testing is used to cut the time required to determine if a coating system offers long-term durability. Accelerated weathering tests are difficult to correlate with natural weathering. However, they can be useful in determining the relative performance of coating systems and when results are combined from several accelerated weathering tests and natural weathering tests, a picture of the long term performance potential for coating systems can often be surmised.

Figure 1 below shows results from the QUV-A weatherability test, ASTM D4587, "Standard Practice Fluorescent **UV-Condensation** for Exposures of Paint and Related Coatings." In this test a coating is exposed to UV light with a single wavelength at 340 nm. Results for several commonly used topcoats are shown below, and are measured by monitoring gloss retention over thousands of hours. Gloss retention is measured according to ASTM D523, "Standard Test Method for Specular Gloss," and results below are reported for a gloss meter geometry of 60°. The test method calls for a 4-hour water condensation cycle with a water temperature of 50 °C.





The drawback of the OUV-A test is that it exposes the coating to only one wavelength of UV light. The UV spectrum of sunlight spans multiple wavelengths, some much more energetic than that in the QUV-A test. Exposure of coatings in the Xenon Arc test chamber in the ASTM D6695 test, "Standard Practice for Xenon-Arc Exposures of Paint and Related Coatings" addresses this issue. Filters on the light source in this test allow light from wavelengths of around 300 nm to 800 nm, which more closely matches the full spectrum of light found in natural sunlight. Water is applied during the dark cycle to simulate humidity and rainfall. Figure 2 below shows comparative results.

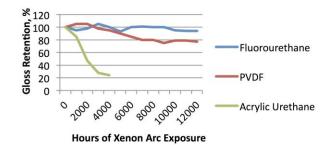


Figure 2: Xenon Arc Weathering of Fluoropolymer Topcoat

While the Xenon Arc test exposes coatings to a light spectrum that closely approximates that of natural sunlight, there are still differences. Natural sunlight is a continuous spectrum, while the Xenon Arc tends to "spike," or let in more light of particular wavelengths. The EMMAQUA (Equatorial Mount with Mirrors for Acceleration with Water, ASTM G90) test uses mirrors to focus natural sunlight onto the surface of coated panels. As in the other accelerated weathering methods, the panels are sprayed periodically with water to simulate rainfall. Unlike most other accelerated weathering methods, EMMAQUA exposes the coated panels to all wavelengths of natural sunlight, theoretically yielding results closer to long term natural exposure. The results of the EMMAQUA test are reported in terms of the total amount of energy per unit area to which the coatings are exposed. Figure 3 below shows EMMAQUA test results for an FEVE coating, a PVDF coating, and an acrylic urethane topcoat.

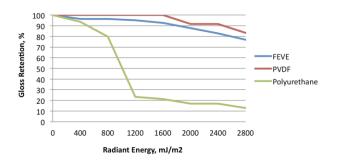


Figure 3: EMMAQUA Accelerated Weathering Test of Fluoropolymer Topcoat

EMMAQUA test results indicate that the two fluoropolymer coatings have the best gloss retention at the end of the test.

Natural Weathering Test Results

Natural weathering of coatings is the preferred method to gauge coating performance. The drawback to natural weathering tests is the long amount of time required to get results. This is especially true of fluoropolymer coatings, which have expected lives of 30 years or more. Natural weathering tests are often run in areas where exposure to UV radiation and corrosion initiators in highest, in order to determine coating performance under the worst possible circumstances. South Florida in the U.S. near the ocean is a common location for natural weathering test sites. In Japan, Okinawa is a preferred location. Both Florida and Okinawa are considered humid subtropical climate zones. Since it would be impossible to obtain complete natural weathering test results for a fluoropolymer coating prior to commercialization, usually some combination of accelerated and natural weathering is performed. Exterior weathering is done using ASTM G7, "Standard Practice for Atmospheric Environmental Exposure Testing of Nonmetallic Materials."

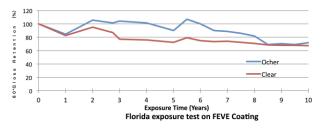


Figure 4: South Florida Weathering Test Results

Figure 4 above shows weathering of a clear and a pigmented FEVE topcoat in South Florida.

The FEVE topcoat shows good gloss retention after 10 years in South Florida.

In Japan, test sites on the island of Okinawa are used for natural weathering. Okinawa is at approximately the same latitude as Jacksonville, FL. Both regions have a humid subtropical climate. Results for an FEVE topcoat are shown below in Figure 5.

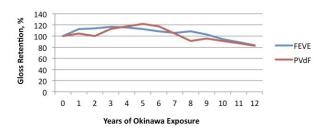


Figure 5: Okinawa Weathering Test Results

Other tests have been performed on FEVE topcoats subjected to natural weathering. Several are discussed below.

Other Test Results⁽³⁾

FEVE coating systems have been tested on an offshore platform in Suruga Bay, Japan. This platform sits 200 meters offshore and is used for testing paints and coatings, plastics, and metals. An FEVE coating system consisting of a zinc rich primer, an epoxy mid coat, and an FEVE topcoat of 25 μ m thickness was placed on the platform alongside a polyurethane coating system with the same topcoat thickness. The panels were left on the platform for 16 years. Topcoat thickness was measured at various intervals and at the completion of the test. Results are summarized below in Table 1.

	Acrylic Urethane Topcoat	FEVE Resin Topcoat
Initial Thickness, µm	25	25
Final Thickness, µm	0 (After 12 years)	21

Table 1: Topcoat Thickness Measurement Results,16 Years of Exposure

The test results show that the urethane topcoat was completely degraded by the end of the 12th year of the test. Basically, UV radiation, salt, oxygen and other degradation initiators broke the urethane polymer into units of smaller and smaller molecular weight. Over time, the low molecular weight decomposition products were washed away by rain and wind, reducing the coating thickness. The elements would have degraded the appearance of the urethane coating long before it disappeared. In contrast, the FEVE topcoat lost only 4 μ m of coating thickness over the 16-year time of the test, or an average of only 0.025 μ m/year. The theoretical life of the 25 μ m topcoat is more than 100 years based on this average degradation rate. Gloss retention for the two coatings was not measured.

Also measured on the platform was the comparative rate and degree of chalking of the urethane and fluorinated topcoats. Chalking results from the accumulation of degraded coating on the surface of the coating; it will show as a white or colored powder on the coating. ASTM D4214. "Standard Test Methods for Evaluating the Degree of Chalking of Exterior Paint Films" was the method used to monitor chalking over the 20 years of the test. Coatings are rated 1-10, with 10 meaning no chalking observed and 0 meaning the coating was completely chalked. Results are shown below in Figure 6.

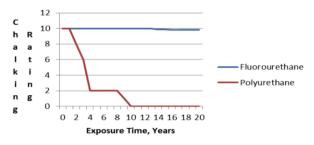


Figure 6: Chalking Test of FEVE Coating Compared to Polyurethane

Figure 6 shows that the polyurethane topcoat starts to chalk severely after only about 4 years. Although the worst chalking doesn't occur until 10 years after initiation of the test, it means the appearance of the polyurethane coating is declining from the first year.

In another exterior test, FEVE and polyurethane coating samples were placed on a rooftop in Hiroshima, Japan in an industrial area for 15 years. A portion of each panel was covered to prevent degradation of the coatings over time and to provide baseline measurements for comparison with the weathered coatings. Photomicrographs of cross sections from each coating sample are shown below in Figure 7.

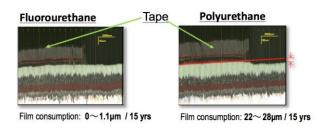


Figure 7: Coating Degradation in an Industrial Area

The photos show that about 1/3 of the polyurethane's original thickness of 75 µm has been lost to degradation. Although part of the coating remains, the appearance of the coating would be poor compared to its initial condition. In contrast, the FEVE fluorinated urethane topcoat has lost very little of its initial thickness of about 50 µm. Losing an average of 0.07 µm/year means that the fluorinated topcoat has a theoretical life exceeding 100 years.

Corrosion Resistance of Fluoropolymer Coatings

As mentioned earlier the primary reason for using coatings on steel bridges is to reduce corrosion. FEVE coatings have been examined in a number of tests, discussed below.

Salt Fog Corrosion Test

The ASTM B-117 Salt Fog Corrosion Test exposes scribed coated panels to a 5% salt solution over a period of time, in this case 2,000 hours. Corrosion is measured by the amount of rust in the scribe and under the coating adjacent to the scribe as well as by blisters formed by corrosion products. ASTM D1654 describes how the scribe is made and how the results of the B117 exposure test should be reported. Using Method 1 of this test, the scribe was scraped with a spatula after exposure, then the amount of creepage noted. The rating is from 0 to 10 where 10 means zero creepage. In this case, fluorourethane, polysiloxane, and polyurethane topcoats were applied over a 75 µm epoxy primer on smooth steel. fluorourethane/polyurethane Results from the comparison are shown below in Figure 8, while the fluorourethane and polysiloxane comparison is shown in Figure 9.



Figure 8: Salt Fog Corrosion Test Results, Polyurethane and Fluorourethane

Left: Polyurethane, Right: Fluorourethane

Both samples show corrosion in the scribe, but the fluorinated coating shows less creepage under the coating. The fluorourethane is rated a 6 on the D1654 scale, while the urethane is rated a 2.



Figure 9: Salt Fog Corrosion Test Results, Polysiloxane and Fluorourethane

Left: Polysiloxane Right: Fluorourethane

The fluorinated urethane is rated a 6 on the scale, while the polysiloxane is rated a 3.

Cyclic Prohesion Corrosion Test

A fluorourethane topcoat system was compared to more conventional coatings in the ASTM D5894 "Cyclic Salt Fog/UV Exposure of Painted Metal." This test exposes coating systems to alternating one week cycles in a fog/dry cabinet and a UV/condensation cabinet. The idea is to better simulate actual environmental conditions to which coatings are exposed. The test uses a 0.5% sodium chloride and 0.35% ammonium sulfate solution at a lower pH than the salt fog test. Results include % gloss retention and mm of scribe creep.⁽⁴⁾ The total length of the test is 5,040 hours; 2,520 in the QUV-A cabinet and 2,520 in the salt fog cabinet.

Three three-coat systems were prepared for testing in the cyclic prohesion test. All systems consisted of an organic epoxy zinc rich primer, a polyamide epoxy intermediate coat, and either a fluorourethane, polysiloxane, or polyurethane topcoat. Results from these three systems are shown below in Table 2.

	Coating Type	60° Gloss Retention (%)	Scribe Creep (mm)
Primer	Organic Zinc Epoxy	NA	NA
Midcoat	Polyamide Epoxy II	NA	NA
Topcoats	Polyurethane	54.3	8
	Epoxy Polysiloxane	72.0	12
	Fluorourethane	91.0	8

Table 2: Comparison of Three Coat Systems in
Cyclic Prohesion

The data in Tables 2 shows the outstanding weatherability of the fluorinated topcoat compared to the polysiloxane and polyurethane products. The corrosion resistance of the polyurethane and fluorourethane coating systems are the same, and both offer an improvement over the polysiloxane.

Three two coat systems were prepared for testing in the cyclic prohesion test. Two-coat systems are becoming more popular in the bridge market because they can be applied in the field or in the shop more quickly than a three-coat system. Test results for the two coat systems are shown below in Table 3.

	Coating Type	60° Gloss Retention (%)	Scribe Creep (mm)
Primer	Organic Zinc Epoxy	NA	NA
Topcoats	Polyurethane	35.6	10
	Epoxy Polysiloxane	52.2	12
	Fluorourethane	73.2	8

Table 3: Comparison of Two Coat Systems in
Cyclic Prohesion

Results again show the improvement in gloss retention offered by the fluorourethane topcoat. The fluorinated product also has corrosion resistance matching or exceeding that of the siloxane and urethane coating systems. Note that the gloss retention of all the coating systems is lower than that of the three-coat systems.

Electrochemical Impedance Spectroscopy (EIS) Test

A comparison of coating systems was also performed in Electrochemical Impedance Spectroscopy (EIS). EIS allows quantitative determination of coating properties without affecting the coating, and enables detection of small changes in coating behavior in a short time period. Organic coatings initially have a high electrical resistance through the coating. As coatings age, the interconnecting porosity in the coating becomes saturated with water, chloride, oxygen and other corrosion initiators⁽⁵⁾. The metal surface is then exposed to corrosion. In this version of the test, the coatings are first weathered in the SWOM (Sunshine Weatherometer) test, and then placed in the salt fog corrosion test. The SWOM test uses a carbon arc light source, which generates a spectrum similar to sunlight but with higher intensity at 350-400 nm. The change in impedance in 100 ohm/cm² is measured for each coating system. The smaller the change in initial impedance, the better the corrosion resistance of the coating system. Figure 10 below shows the test results.

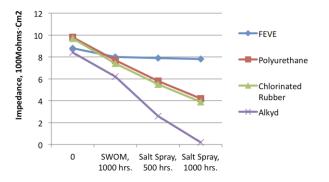


Figure 10: Electrochemical Impedance Spectroscopy Test Results

According to some sources, coatings with an impedance of >108 ohm/cm² provide excellent corrosion protection, while those with <106 ohm/cm² are said to provide poor corrosion protection⁽⁶⁾. All of the coatings in the test start above an impedance of 108. As the polyurethane, chlorinated rubber and alkyd coatings are exposed to degradation in the SWOM test and in the salt fog test, their impedance gradually drops, in the case of the alkyd, to zero. The impedance of the FEVE coating was virtually unchanged over the test cycle, indicating that the coating retained its corrosion resistance.

Earlier test results indicated that FEVE-based coatings retain coating thickness over long periods of time. This property is not only important for the appearance of the coating over time but also for the corrosion resistance of the coating system. Zinc rich primers, used since the 1970's, directly protect steel by corroding preferentially when in contact with corrosion initiators like chloride ion. Epoxy or urethane intermediate coats provide additional coating thickness that makes damaging the coating more difficult. Topcoats also provide coating thickness. The advantage of FEVE topcoats is that they remain intact for far longer periods than conventional coatings, making it more difficult for corrosion initiators to penetrate to the steel substrate.

Bridge Coating Specifications in Japan

1990 Japanese National Specification for Steel Bridge Coatings⁽⁷⁾

Based on years of field experience and accelerated weathering and corrosion testing on FEVE resin-

based coatings, the first Japanese National Specification for bridge coatings was developed in 1990. That specification is shown below in Table 4.

		ENVIRONMENT		
		General	Slightly Severe	Severe
Coating Type		No salt or corrosives Non-industrial areas Little smog Easy to recoat	Salt used in area Slight pollution Moderate smog Difficult to recoat	High salt levels Severe pollution Heavy smog Difficult to recoat
	General Purpose Coating	A-1, A-2	B-1	C-1, C-2
	High Durability Coating	A-3, A-4	C-3, C-4	

Table 4: 1990 Japanese National Specification for
Steel Bridge Topcoats⁽⁸⁾

A-1, A-2: Long oil alkyd coatings

A-3, A-4: Silicone alkyd coatings

B-1: Chlorinated rubber coating

C-1, C-2: Polyurethane coatings

C-3: Fluoropolymer coating, fabricator applied (some components coated on site)

C-4: Fluoropolymer coating, fabricator applied

In this specification, less durable coatings were specified for use in most environments, including bridges with high levels of salt, pollution, and difficulty in recoating. The fluoropolymer topcoats were recommended for use in slightly severe and severe environments when higher durability was desired.

2005 Japanese National Specification for Steel Bridge Topcoats⁽⁸⁾

Based on weathering and corrosion testing, some of which is shown earlier in this paper, in 2005 the specification was revised. Field performance of the fluorourethane coating systems was also considered in the new standard. The updated specification required the use of fluoropolymer topcoats in all environments and for both new construction and field repair on steel bridges. Table 5 below shows these changes.

		ENVIRONMENT		
		General	Slightly Severe	Severe
Application		No salt or corrosives Non-industrial areas Little smog Easy to recoat	Salt in environment Slight pollution Moderate smog Difficult to recoat	High salt levels Severe pollution Heavy smog Difficult to recoat
	New Construction, Shop Application			mer Topcoat
	Repair Coatings, Field Application	Rc-I, RC-III, Fluoropolymer Topcoat		

Table 5: 2005 Japanese National Specification forSteel Bridge Topcoats

The changes to the 2005 specification included the requirement to use fluoropolymer topcoats in all environments due to their superior weathering. Also included was a specification for field application of fluoropolymer topcoats. This meant that existing bridges could now be repainted using the fluoropolymer topcoats.

Life Cycle Cost Analysis of Fluoropolymer Coatings⁽⁹⁾

Based on labor and material costs averaged over several bridge coating projects in Japan using an exchange rate of 120 Japanese yen per U. S. dollar, a life cycle cost comparison for a polyurethane, and a fluorourethane coating system was performed. No discount rate was applied to the costs. Results are shown below in Tables 6 and 7

Topcoat Type	Topcoat Thickness, μm	Topcoat Cost, \$/m ²	
Polyurethane	55	\$4.08	
Fluorourethane	55	\$12.01	

Table 6: Topcoat Cost Comparison

Based on these cost comparisons, it is roughly 3X more expensive initially to use the fluorinated topcoat than the polyurethane. However, when choosing a coating system, not only the topcoat cost but also the applied cost of the entire coating system must be considered. Table 7 shows a comparison of applied and life cycle costs for each coating system.

Coating System	Polyurethane	Fluorourethane	
Total Repainting Cost, \$/m ²	85.65	93.87	
Estimated Coating Life, Years	18	30	60
Total Applied Coating System Cost, \$/m ² /year	4.76	3.13	1.56
Cost Index	48	32	16

Table 7: Applied Coating System Cost and LifeCycle Cost Comparison

Each topcoat is part of a coating system including a primer, intermediate coat, and topcoat.

The cost of the primer and middle coat are the same regardless of the topcoat used. The cost of labor, staging, fuel, and time is also about the same regardless of the coating system chosen. The real difference between the coating systems is the cost of the topcoat. When these additional costs are taken into account, total repainting costs for each system are not that different. The fluorinated urethane is only about 10% more expensive than the urethane. The true cost of the coating system is given by the metric of $m^2/year$. When the time factor is added, the advantage of the fluorinated coating becomes apparent. The fluorinated coating system is 33-67% less expensive than the urethane system, which is the

most commonly used system in the U.S. In the U. S. the cost of the fluorinated paint is higher than in Japan. Even if the cost of the fluoropolymer topcoat doubles to $24.01/m^2$, the life cycle cost advantage remains.

Conclusions

Based on years of field experience and accelerated testing, the Japanese highway authorities have made the use of fluoropolymer topcoats mandatory on steel bridges. The use of these topcoats offers substantial life cvcle cost advantages over conventional topcoats, and can substantially reduce the need and cost for maintenance painting. This means over the life of the structure far fewer maintenance cycles will be required, not only reducing direct costs but also the cost of increased traffic and delays caused by maintenance. There is a great deal of evidence that FEVE-based coatings offer good gloss and color retention for up to 60 years, and some experimental evidence they can offer protection for 100 years. In any case, these fluoropolymer topcoats provide the best match between coating system life and asset life available today.

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